

DESIGN & ENGINEERING GUIDE SOLARMOUNT: FLUSH-TO-ROOF DESIGN



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GETTING STARTED - INTRODUCTION DESIGN & ENGINEERING GUIDE PAGE

Getting Started - Introduction

This manual is for professional engineers and permitting authorities. For assistance with your array's engineering and a Bill of Materials, see our U-Builder at http://design.unirac.com

SOLARMOUNT Flush-to-Roof is an extruded aluminum rail system that is engineered to hold most framed solar modules to a roof structure and installed parallel to the roof. With SOLARMOUNT, you'll be able to solve virtually any PV module mounting challenge.

Some of the features of this product include:

- Integrated Full System Grounding and Bonding to UL 2703
 - o Integrated Bonding Rail Splice
 - o Integrated Bonding Module Midclamp Assembly
 - o Module Endclamp Assembly
 - Bonding Microinverter Mounting Bolt Assembly
 - o Integrated Bonding L-Foot T-Bolt
- Module Landscape (with rails running north/south) or Portrait (with rails running east/west) Orientations
- Works with Most Framed Modules
- Wire Management Clip
- Designed per the ASCE 7-05 and ASCE 7-10 Building Code
- Component Testing
- Rigorous Engineering Analysis
- Superior Aesthetics
 - o Optional Front Trim
 - Optional End Caps (SOLARMOUNT Standard and Light Rail Only)



Installer Responsibility & Disclaimer

Please review this guide and the SOLARMOUNT Installation Guide thoroughly before installing your SOLARMOUNT system. These guides provide supporting documentation for building permit applications, planning, and assembling the SOLARMOUNT system.

The installer is solely responsible for:

- Complying with all applicable local or national building codes, including code requirements that can be more stringent than the guidelines set forth in this manual;
- Maintaining and enforcing all aspects of a safe working environment;
- Ensuring that Unirac and other products are appropriate for the particular installation and the installation environment;
- Ensuring that the roof, its rafters, connections, and any other structural support members can support the array under all code level loading conditions (this total building assembly is referred to as the building structure);
- Using only Unirac parts and installer-supplied parts as specified by Unirac (substitution of parts may void the warranty and invalidate the letters of certification in all Unirac publications);
- Ensuring that lag screws have adequate pullout strength and shear capacities as installed;
- Verifying the strength of any alternate mounting if used in lieu of the lag screws;
- Maintaining the waterproof integrity of the roof, including selection and proper installation of appropriate flashing;
- Ensuring safe installation of all electrical aspects of the PV array, including proper grounding/bonding;
- Array shading and output analysis;
- Ensuring correct and appropriate design parameters are used in determining the design loading used for design of the specific installation. Parameters, such as snow loading, wind speed, exposure and topographic factor should be confirmed with the local building official or a licensed professional engineer.

Unirac shall not be liable for any losses, damages, or injuries that directly or indirectly result from any non-conformance with the above.



Design Methodology

SOLARMOUNT was designed using the *Minimum Design Loads for Buildings and Other Structures* by the *American Society of Civil Engineers and Structural Engineering Institute*, 2005 and 2010 editions. These are referred to as ASCE 7-05 and ASCE 7-10, respectively. Three methods have been provided to aid in design of your project. The use of these methods is discussed in the *Project Requirements & Design Aid* section in the next page.

Quick Note – The online U-Builder is highly recommended for all qualifying projects. It will provide you with a Bill of Materials, Certification Letter, and Calculations for your project. Please review Table 1 in the *Project Requirements and Design Aid* section of this Guide.



Project Requirements & Design Aid

Table 1 - Project Requirements & Design Aid							
Project Require (Blank Cells for Project Specific In Convenience)	out Provided for your	Design Aid					
Project Name: Project Address: AHJ (Authority Having Jurisdiction):			ilder ^{1a} esign Tool)	-	ve Design lod ^{1b}		ourself ^{1c} al Method)
Current Adopted Building Code: Local Jurisdiction Code Amendments:		ASCE 7-05	ASCE 7-10	ASCE 7-05	ASCE 7-10	ASCE 7-05 ASCE 7-2	
Occupancy/Risk Category*: Basic Wind Speed*:			l 110-170 mph		***	As Permitte	ed by Code ed by Code
Wind Exposure Category*: Ground Snow Load*:		0-60	or C) psf	*:	or D **	As Permitted by Code As Permitted by Code	
Seismic Coefficient, Ss*: Roof Height (Eave & Ridge)*:		\leq 3.1g \leq 3.1g As Permitted \leq 30 feet \leq 60 feet As Permitted		ed by Code			
Roof Slope*: Roof Zone(s)*:		0-45 Degrees 0-45 Degrees As Permitted 1, 2, or 3 1, 2, and 3 As Permitted		ed by Code			
Framed Module Type & Module*: Module Weight*:		User Input Most 60 and 72 Cell User Ir Module Dependent See Appendix E User Ir		Input			
Module Dimensions*: Total Module Quantity*:		Up to	ependent 50 x 50	Unlir	Dependent User Input User Input User Input		Input
Design Method: Project Specific Calculations for Solar System Provided:		Υ	tress Design es	N	tress Design lo	N	
Stamped/Certified Engineering Letter for Solar System Provided: Bill of Materials for Unirac Components of Solar System Provided: * Requirements must fall within defined range to utilize specified design aid.			es es	N N	es lo	N N	lo lo

^{*} Requirements must fall within defined range to utilize specified design aid.

The U-Builder allows for a customized project design that results in a final design, bill of materials, price guote and stamped/certified engineering approval letters.

^{**} The design professional could use the appropriate code to perform the design in LRFD, LSD, or ASD. The ASD procedure for the Analytical Method has been provided.

^{***} Prescriptive Pressure tables located in Appendix B and Online. Pressure Tables exist for Basic Wind Speeds of 85-170 mph for ASCE 7-05 and 110-190 mph for ASCE 7-10.

¹a. U-Builder: This is an easy-to-use online design tool that is recommended for all preliminary and final designs, estimating, and layout validation. It is located on our website at www.unirac.com.

<u>1b.</u> Prescriptive Design Method: This method is a simplified approach to the design of your SOLARMOUNT project. This method is recommended when computers or internet access is not available. Once project specific requirements are known, the project design load pressures can be looked up in the Pressure Lookup Tables located in Appendix B. If additional tables are needed, they can be found online at www.unirac.com.

¹c. Do It Yourself (Analytical Method): This design approach follows the ASD calculations step by step through both the ASCE 7-05 and 7-10 design codes. Equations, figures, tables, and commentary are provided for your convenience to aid in generating the specific design load pressures for your loading conditions, such as wind and snow. This method has been provided for design or layout requirements that fall outside of the other two options or for design professionals that prefer to perform their own calculation package.



PRESCRIPTIVE DESIGN METHOD DESIGN & ENGINEERING GUIDE

Prescriptive Design Method - Quick Design Steps

Step 1: Define Project Requirements

- a. Fill in the Table 1 Project Requirements & Design Aid on previous page.
- b. Once project specific information is determined, confirm that the Prescriptive Design Method may be utilized.
- c. Review the Prescriptive Pressure Tables in the Appendix to see if they meet your needs. If a more precise design is needed (if the tables in the Appendix don't meet your project requirements, but per Table 1, you can still utilize the Prescriptive Design Method) please utilize the online tool for design.

Step 2: Create Initial Array Layout

- a. Identify the structural supporting members of your building. A sketch/drawing of the roof/building with location of supporting members, vents, skylights, cable/wires, areas to avoid, etc., is highly recommended.
- b. Create a "rough draft" layout of solar modules on the actual project roof. (Refer to the SOLARMOUNT Installation Guide.)



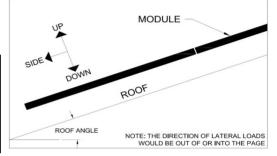
PRESCRIPTIVE DESIGN METHOD DESIGN & ENGINEERING GUIDE

Step 3: Determine Array Design Pressure by Roof Zone to Select a Rail Span

- a. Using information in Steps 1 & 2, select a Prescriptive Pressure Table contained Appendix B or online.
- b. Use fill-in boxes below to document your project specific pressures and tables utilized.

Pressure Table Used: Controlling Pressure: Basic Wind Speed Building Height Exposure Category Seismic Coefficient (Ss) Roof Pitch Ground Snow Load Controlling Pressure: Roof zone 1: Roof zone 2: Roof zone 3:

	Up (psf)	Down (psf)	Side (psf)	Lateral (psf)
Roof zone 1:				
Roof zone 2:				
Roof zone 3:				
'-				



Note: For Low Profile Mode, where rails are perpendicular to the roof tilt (E-W Rails), "Side Load" (Down Slope) is load applied in weak axis bending of the SOLARMOUNT rail along the roof tilt and "Lateral" is load applied as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt. For High Profile Mode, where rails are parallel to the roof tilt (N-S Rails), "Side Load" (Downslope) is load applied in as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt and "Lateral Load" is applied in weak axis bending of the SOLARMOUNT rail along the roof tilt.

- Convert pressures (lbs/ft² or psf) from the boxes just filled in to pounds per linear foot (lb/ft or plf) using the following steps:
 - i. Pressure (from table above) * Area of Module = Total Pounds per Module
 - ii. Total Pounds Per Module / 2 (Number of rails) = Pounds Per Rail
 - iii. Pounds Per Rail / Width of Module Parallel with the Rail = Pounds per Linear Foot (plf)
- d. Use the *Downward and Upward Span Length Tables* in Appendix C with the plf loads to determine maximum spans.
 - i. Look up the table "Downward Span Lengths". Using the "Down" plf load and the "Side" plf load combinations, choose the maximum span length in the table.
 - ij. Look up the table "Uplift Span Lengths" and using the "Up" plf and "Side" plf load combinations to choose the maximum span length.
 - iii. Use the smaller length of the "Down" and "Up" maximum span length.
 - iv. Cantilever (overhang) lengths can be up to 33% of the span length. For example, a 9 foot span length can have a 3 foot cantilever. The cantilever is defined as the distance from the center of a L-Foot to the edge of a rail.



PRESCRIPTIVE DESIGN METHOD DESIGN & ENGINEERING GUIDE

Step 4: Determine Load to the Roof

*The U-Builder online can automatically calculate maximum point loads to the roof.

- a. To determine the load on the roof through the attachment:
 - i. Determine the tributary area to each attachment.
 - ii. Review the controlling pressure in Step 3b.
 - iii. Determine pressure zones on the roof per ASCE 7-05, Figure 6-3 or ASCE 7-10, Figure 30.5-1.
 - iv. Multiply the tributary area by the roof pressure to obtain loads to the roof attachment.
 - v. Determine the point load to the roof at each attachment.

Step 5: Check Roof Load

a. Ensure that the supporting structure is capable of withstanding the additional loads imposed by the proposed solar system.

Step 6: Check the Connections

- a. Similar to Step 3c, determine the tributary area to each connection and the applied load from the Controlling Pressures table in Step 3.
- b. Convert the applied psf loads into pounds through tributary area.
- c. Look up the Technical Data Sheets in Appendix G for maximum permissible load to each connection.
- d. From Step 4, determine if the attachment (lag bolt or other appropriate attachment) is capable of withstanding the point loads applied.
- e. If the maximum permissible load is greater than the applied load, then the connections are adequate.

Step 7: Define Grounding and Bonding Path

a. Refer to the Installation Guide for how to determine the Grounding and Bonding Path.

Step 8: SOLARMOUNT Front Trim Check

a. SOLARMOUNT Front Trim should not be installed in areas where the wind load exceeds 100 psf, where the distance from clamp to clamp (span) exceeds 52 inches, or where the cantilever (overhang) is greater than 66% of the span length. To determine your pressure, please use Appendix B. You will need to review the table assosciated with your project wind speed and no snow, and review the Up and Down Loads (psf) to determine if SOLARMOUNT Front Trim is appropriate for your project.



ASCE 7-05 Analytical Method

Step 1: **User Inputs (ASCE 7-05)**

Roof Height (ft):	Mean roof height (15 ft, 30 ft, or 60 ft)
Roof Angle (degrees):	Convert roof pitch to angle in degrees [See Appendix D]
Basic Wind Speed (mph):	Per Basic Wind Speed - US Map (ASCE 7-05, Figure 6-1)
Wind Exposure Category:	Determine the Exposure Category (B, C or D) by using the definitions for Surface Roughness Categories (ASCE 7-05, Sections 6.5.6.2 and 6.5.6.3)
Roof Zone:	Determine the Roof Zone (1, 2 or 3) (ASCE 7-05, Figure 6-3)
Ground Snow Load (psf):	Pg = Ground Snow Load in psf. Ground Snow Loads (ASCE 7-05, Figure 7-1)
Seismic Coefficient Ss (g):	ASCE 7-05 (Figures 22-1, 22-3, 22-5, 22-7, 22-9 through 22-11, 22-13, and 22-14)
Roof Live Load ¹ (psf):	0 psf, 20 psf, etc.
Module Manufacturer/Type:	
Solar Module Length (in):	
Solar Module Width (in):	
Solar Module Weight (lb):	
Module Dead Load (psf)	

Commentary:

1) Most Building Officials allow for all or a portion of the roofs original live load design load to be removed/reduced at the time that solar panels are being added to the roof. The rationale behind this is that live load or roof foot traffic is eliminated or reduced to designated paths. in other words, the roof top solar array and live load foot traffic cannot occupy the same space. If all of the roof live load can be utilized by the proposed solar array, 0 psf should be entered.



<u>Step</u> 2: Wind Pressure (ASCE 7-05, Chapter 6)

Wind Pressure Equation	- Method 2 - Analytical F	Procedure (ASCE 7-05, Section 6.5):				
Pp=qh ((GCpp-GCpi) (ASCE 7-0	5, Section 6.5.12.4.1) (GCpp - Positive Downforce Factor)				
Pn=qh ((GCpn-GCpi) (ASCE 7-0	5, Section 6.5.12.4.1) (GCpn - Negative Uplift Factor)				
	Gcpi equals zero (per AC428, November 2012) (internal pressure coefficient)					
		w (ASCE 7-05 Figure 6-11) and is a function of the roof area (feet squared), and roof angle (degrees) (external				
	GCpp (P	ositive downforce factor)				
	GCpn (N	legative uplift factor)				
	(ASCE 7	-05, Figure 6-11B) for roof angles ≤ 7°				
	(ASCE 7	-05, Figure 6-11C) for roof angles > 7° and ≤ 27°				
	(ASCE 7	-05, Figure 6-11D) for roof angles > 27° and ≤ 45°				
	qh = qz					
	qz=0.00256Kz*Kzt*k	(d*V^2*I (ASCE 7-05, Section 6.5.10)				
	Kz	Velocity Pressure Coefficient (ASCE 7-05, Table 6-3)				
Kzt Topographic Factor (ASCE 7-05, Section 6.5.7.1 & Figure 6-4)						
	Kd	Directionality Factor (ASCE 7-05, Table 6-4)				
V Basic Wind Speed in MPH from User Inputs in Step 1						
	I	Importance Factor ² (ASCE 7-05, Table 6-1)				

Calculate the wind pressure for uplift and downforce, using GCpn & GCpp respectively, in the provided boxes.

Commentary:

2) Typical values for the Importance Factor are 0.87 based on Occupancy Category I and 1.0 based on Occupancy Category II. Occupancy I is defined by ASCE 7-05 to mean "Buildings and other structures that present a low hazard to human life in the event of failure...". Occupancy II is defined by ASCE 7-05 to mean "All buildings and other structures except those listed in Occupancy Categories I, III, and IV".



ASCE 7-05 ANALYTICAL METHOD

Dead Load Step 3:

Module Dead Load (psf) should be determined from User Inputs in Module Dead Load (psf): Step 1 [See Appendix E] (The racking system dead load should be taken Racking System Dead as the total weight of the racking system (hardware, rails, nuts, bolts, Load³ (psf): attachments, etc.) divided by the total module area of the system.) Component weights can be found in the technical datasheets. Total Dead Load (psf): Sum of Module Dead Load and Racking System Dead Load

Calculated Dead Load in the provided boxes.

Snow Load (ASCE 7-05, Chapter 7) Step 4:

Sloped Roof Snow Load Pressure Equation:

Ps=0.7*Cs	Ce*Ct*I*Pg	(ASCE 7-05, Section 7.3)
	Pg	Ground Snow Load ⁴ (psf) from User inputs in Step 1
	Cs	Slope Factor (ASCE 7-05, Figure 7-2)
	C_t	Thermal Factor ⁵ (ASCE 7-05, Table 7-3)
	I	Importance Factor ⁶ (snow) (ASCE 7-05, Table 7-4)
	Ce	Exposure Factor (ASCE 7-05, Table 7-2)

Calculate Ps (Sloped roof snow load) in the provided boxes.

Commentary:

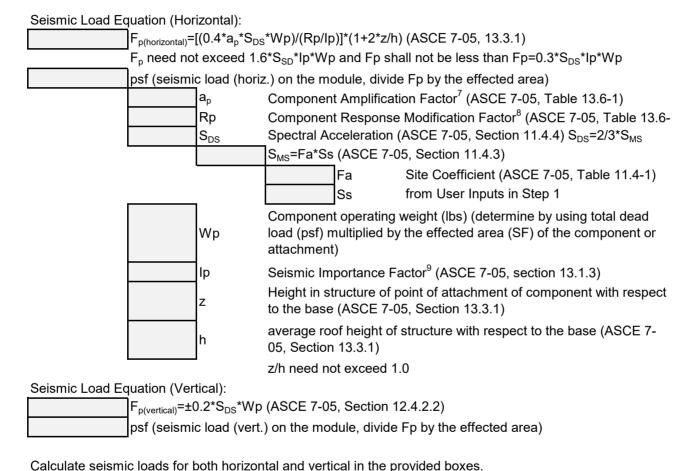
- 3) To be combined with the module dead load and used in wind load combinations.
- 4) The ground snow load is utilized to calculate the roof snow load, which is the load applied to the structure.
- 5) From Section C7.8 of ASCE 7-05, "the collectors should be designed to sustain a load calculated by using the "unobstructed slippery surfaces" curve in Fig. 7-2a". This graph recommends the use of a Ct value of less than or equal to 1.0.
- 6) The Snow Importance Factor for Occupancy Category I = 0.8 and for Occupancy Category II = 1.0.



ASCE 7-05 ANALYTICAL METHOD

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Step 5: Seismic Load (ASCE 7-05)



Commentary:

- 7) The Component Amplification Factor (ap) for flush-mount systems should be taken as 1.0 (International Code Council (ICC) Acceptanc Criteria (AC) 428, Section 3.1.3.3).
- 8) The Component Response Modification Factor (Rp) for flushmount systems should be taken as 1.5 (International Code Council (ICC) Acceptanc Criteria (AC) 428, Section 3.1.3.3).
- 9) The Seismic Importance Factor for Occupancy Categories I and II = 1.0.



Step 6: Rewrite Your Loads

*Depending on your coordinate system, certain loads will need to be split into their horizontal and vertical components.

Total Dead Load:	psf
Wind Pressure Up:	psf
Wind Pressure Down:	psf
Snow Load:	psf
Seismic Load Horizontal:	lbs
Seismic Load Vertical:	psf

Step 7: Allowable Stress Design (ASD) Load Combinations (ASCE 7-05, Chapter 2, Section 2.4.1)

*The load combinations below have been identified as the likely controlling cases for the roof structure.

1) D

2) D + Lr

3) D + S

4) D + W_{up}

5) D + W_{down}

6) D + $0.75W_{down}$ + 0.75S

7) D + $0.75W_{down}$ + 0.75Lr

8) D + 0.75(0.7E) + 0.75Lr

9) D + 0.75(0.7E) + 0.75S

10) D + 0.7E

11) $0.6D + W_{up}$

12) $0.6 D + W_{down}$

13) 0.6 D + 0.7E

D = Dead Load

Lr = Live Load to Roof

S = Snow Load

W_{up} = Wind Load Up

 W_{down} = Wind Load Down

E = Earthquake/Seismic Load

Step 8: Create Initial Array Layout

- a. Identify the structural supporting members of your building. A sketch/drawing of the roof/building with location of supporting members, vents, skylights, cable/wires, areas to avoid, etc., is highly recommended.
- b. Create a "rough draft" layout of solar modules on the actual project roof. (Refer to the SOLARMOUNT Installation Guide.)



ASCE 7-05 ANALYTICAL METHOD DESIGN & FINGING GILLDE

Step 9: Determine a Rail Span

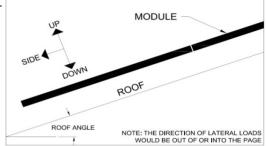
*For structural engineers who would like to determine the rail span without utilizing the Prescriptive Method, section properties can be found in Appendix F - Technical Data Sheets.

- a. Using information in Step 1 & 8, select a Prescriptive Pressure Table contained the Appendix B or
- b. Use fill-in boxes below to document your project specific pressures and tables utilized.

Pressure Table Used: Controlling Pressure: Basic Wind Speed - Building Height - Roof zone 1:

Building Height
Exposure Category
Lateral (Ss)
Roof Pitch
Ground Snow Load -

J				
	Up (psf)	Down (psf)	Side (psf)	Lateral (psf)
Roof zone 1:				
Roof zone 2:				
Roof zone 3:				
•	Alite Field	D ("L . 1.4.		1



Note: For Low Profile Mode, where rails are perpendicular to the roof tilt (E-W Rails), "Side Load" (Down Slope) is load applied in weak axis bending of the SOLARMOUNT rail along the roof tilt and "Lateral" is load applied as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt. For High Profile Mode, where rails are parallel to the roof tilt (N-S Rails), "Side Load" (Downslope) is load applied in as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt and "Lateral Load" is applied in weak axis bending of the SOLARMOUNT rail along the roof tilt.

- c. Convert pressures (lbs/ft² or psf) from the boxes just filled in to pounds per linear foot (lb/ft or plf) using the following steps:
 - i. Pressure (from table above) * Area of Module = Total Pounds per Module
 - ii. Total Pounds Per Module / 2 (Number of rails) = Pounds Per Rail
 - iii. Pounds Per Rail / Width of Module Parallel with the Rail = Pounds per Linear Foot (pl
- d. Use the Downward and Upward Span Length Tables in Appendix C with the plf loads to determine maximum spans.
 - i. Using the plf loads for "Down", look up the table "Downward Span Lengths" in Appendix B and using the "Down" plf load and the "Side" plf load combinations to choose the maximum span length.
 - ii. Using the plf loads for "Up", look up the table "Uplift Span Lengths" in Appendix and using the "Up" plf and "Side" plf load combinations to choose the maximum span length.
 - iii. Use the smaller length of the "Down" and "Up" maximum span length.
 - iv. Cantilever (overhang) lengths can be up to 33% of the span length. For example, a 9 foot span length can have a 3 foot cantilever. The cantilever is defined as the distance from the center of a L-Foot to the edge of a rail.



Step 10: Look-up Layout and Attachment Guidelines for Array

a. Review your layout in Step 8 above and the Layout and Attachment Guidelines to determine potential attachment points to your structure.

Step 11: Determine Load to the Roof

- a. To determine the load on the roof through the attachment:
 - i. Determine the tributary area to each attachment.
 - ii. Review the controlling pressure in Step 9.
 - iii. Determine pressure zones on the roof per ASCE 7-05, Figure 6-3.
 - iv. Multiply the tributary area by the roof pressure to obtain loads to the roof attachment.
 - v. Determine the point load to the roof at each attachment.

Step 12: Check Roof Load

a. Ensure that the supporting structure is capable of withstanding the additional loads imposed by the proposed solar system.

Step 13: Check the Connections

- a. Similar to Step 9c, determine the tributary area to each connection and the applied load from the Controlling Pressures table in Step 9
- b. Convert the applied psf loads into pounds through tributary area.
- c. Look up the Technical Data Sheets in Appendix H for maximum permissible load to each connection.
- d. From Step 11, determine if the attachment (lag bolt or other appropriate attachment) is capable of withstanding the point loads applied
- e. If the maximum permissible load is greater than the applied load, then the connections are adequate.

Step 14: Define Grounding and Bonding Path

a. Refer to the SOLARMOUNT Installation Guide for how to determine the Grounding and Bonding Path.

Step 15: SOLARMOUNT Front Trim Check

a. SOLARMOUNT Front Trim should not be installed in areas where the wind load exceeds 100 psf, where the distance from clamp to clamp (span) exceeds 52 inches, or where the cantilever (overhang) is greater than 66% of the span length. Please review the Step 6 Up and Down Wind Loads (psf) to determine if Front Trim is appropriate for your project.



ASCE 7-10 Analytical Method

Step 1: **User Inputs (ASCE 7-10)**

_	Notes / Clarifications:
Roof Height (ft):	Mean roof height (15 ft, 30 ft, or 60 ft)
Roof Angle (degrees):	Convert roof pitch to angle in degrees [See Appendix D]
Risk Category:	Table 1.5-1
Basic Wind Speed (mph):	Per Basic Wind Speeds for Risk Category II (ASCE 7-10, Figure 26.5-1A)
Wind Exposure Category:	Determine the Exposure Category (B, C or D) by using the definitions for Surface Roughness Categories (ASCE 7-10, Sections 26.7.2 and 26.7.3)
Roof Zone:	Determine the Roof Zone (1, 2 or 3) (ASCE 7-10, Figure 30.5-1)
Ground Snow Load (psf):	Pg = Ground Snow Load in psf. Ground Snow Loads (ASCE 7-10, Figure 7-1)
Seismic Coefficient Ss (g):	ASCE 7-10 (Figures 22-1, 22-3, 22-5, 22-6 and 22-17)
Roof Live Load ¹ (psf):	0 psf, 20 psf, etc.
Module Manufacturer/Type:	
Solar Module Length (in):	
Solar Module Width (in):	
Solar Module Weight (lb):	
Module Dead Load (psf)	

Notes / Clarifications:

Commentary:

1) Most Building Officials allow for all or a portion of the roofs original live load design load to be removed/reduced at the time that solar panels are being added to the roof. The rationale behind this is that live load or roof foot traffic is eliminated or reduced to designated paths. in other words, the roof top solar array and live load foot traffic cannot occupy the same space. If all of the roof live load can be utilized by the proposed solar array, 0 psf should be entered.



Step 2: Wind Pressure (ASCE 7-10, Chapter 30)

Wind Pressure Equation - 0	Components & Clado	ling (ASCE 7-10, Section 30.4.2):			
Pp=qh (G	Pp=qh (GCpp-GCpi) (ASCE 7-10, Section 30.4.2) (GCpp - Positive Downforce Factor)				
Pn=qh (G	Cpn-GCpi) (ASCE 7-	10, Section 30.4.2) (GCpn - Negative Uplift Factor)			
	Gcpi equals zero (p	per AC428 - Nov, 2012) (internal pressure coefficient)			
	GCp is defined below (ASCE 7-10 Figure 30.4-2) and is a function of the roof zone, effective wind area (feet squared), and roof angle (degrees) (external pressure coefficient)				
	GCpp (Positive downforce factor)			
	GCpn (Negative uplift factor)			
	(ASCE	7-10, Figure 30.4-2A) for roof angles ≤ 7°			
	(ASCE	7-10, Figure 30.4-2B) for roof angles > 7° and ≤ 27°			
	(ASCE	7-10, Figure 30.4-2C) for roof angles > 27° and ≤ 45°			
	qh = qz				
	qz=0.00256*Kz*Kz	t*Kd*V^2 (ASCE 7-10, Section 30.3.2)			
	Kz	Velocity Pressure Coefficient (ASCE 7-10, Table 30.3-1)			
	Kzt	Topographic Factor (ASCE 7-10, Section 26.8 & Figure 268-1)			
	Kd Directionality Factor (ASCE 7-10, Table 26.6-1)				
	V	Basic Wind Speed in MPH from User Inputs in Step 1			

Calculate the wind pressure for uplift and downforce, using GCpn & GCpp respectively, in the provided boxes.



Dead Load Step 3:

Module Dead Load (psf): Module Dead Load (psf) should be determined from User Inputs in Step 1 Racking System Dead [See Appendix E] (The racking system dead load should be taken as the total weight of the racking system (hardware, rails, nuts, bolts, Load² (psf): attachments, etc.) divided by the total module area of the system.)Component weights can be found in the technical datasheets Total Dead Load (psf): Sum of Module Dead Load and Racking System Dead Load

Calculated Dead Load in the provided boxes.

Snow Load (ASCE 7-10, Chapter 7) Step 4:

Sloped Roof Snow Load Pressure Equation:

Ps=0.7*Cs	*Ce*Ct*I*Pg	(ASCE 7-10, Sections 7.3 & 7.4 Flat and Sloped Roof Snow Load)
	Pg	Ground Snow Load ³ (psf) from User inputs in Step 1.
	Cs	Slope Factor (ASCE 7-10, Figure 7-2)
	C _t	Thermal Factor (ASCE 7-10, Table 7-3)
	I	Importance Factor ⁴ (snow) (ASCE 7-10, Table 1.5-2)
	Се	Exposure Factor (ASCE 7-10, Table 7-2)

Calculate Ps (Sloped roof snow load) in the provided boxes.

Commentary:

- 2) To be combined with the module dead load and used in wind load combinations.
- 3) The ground snow load is utilized to calculate the roof snow load, which is the load applied to the structure.
- 4) The Snow Importance Factor for Occupancy Category I = 0.8 and for Occupancy Category II = 1.0.



Seismic Load Equation (Horizontal):

ASCE 7-10 ANALYTICAL METHOD

Step 5: Seismic Load (ASCE 7-10)

$|F_{p(horizontal)}| = [(0.4*a_p*S_{DS}*Wp)/(Rp/Ip)]*(1+2*z/h) (ASCE 7-10, 13.3.1)$ F_n need not exceed 1.6*S_{SD}*Ip*Wp and Fp shall not be less than Fp=0.3*S_{DS}*Ip*Wp psf (seismic load (horiz.) on the module, divide Fp by the effected area) Component Amplification Factor⁵ (ASCE 7-10, Table 13.5-1) Component Response Modification Factor⁶ (ASCE 7-10, Table 13.5-Rp Spectral Acceleration (ASCE 7-10, Section 11.4.4) S_{DS}=2/3*S_{MS} S_{DS} S_{MS}=Fa*Ss (ASCE 7-10, Section 11.4.3) Site Coefficient (ASCE 7-10, Table 11.4-1) from User Inputs in Step 1 Ss Component operating weight (lbs) (determine by using total dead load (psf) multiplied by the effected area (SF) of the component or αW attachment) Seismic Importance Factor (ASCE 7-10, section 1.5-2) lp Height in structure of point of attachment of component with respect to the base (ASCE 7-10, Section 13.3.1) Average roof height of structure with respect to the base (ASCE 7-10, Section 13.3.1) z/h need not exceed 1.0 Seismic Load Equation (Vertical): $|F_{p(vertical)}|$ =±0.2*S_{DS}*Wp (ASCE 7-10, Section 12.4.2.2) psf (seismic load (vert.) on the module, divide Fp by the effected area)

Calculate seismic loads for both horizontal and vertical in the provided boxes.

Commentary:

- 5) The Component Amplification Factor (ap) for flush-mount systems should be taken as 1.0 (International Code Council (ICC) Acceptanc Criteria (AC) 428, Section 3.1.3.3).
- 6) The Component Response Modification Factor (Rp) for flushmount systems should be taken as 1.5 (International Code Council (ICC) Acceptanc Criteria (AC) 428, Section 3.1.3.3).
- 7) The Seismic Importance Factor for Occupancy Categories I and II = 1.0.



Step 6: Rewrite Your Loads

*Depending on your coordinate system, certain loads will need to be split into their horizontal and vertical components.

Total Dead Load:	psf
Wind Pressure Up:	psf
Wind Pressure Down:	psf
Snow Load:	psf
Seismic Load Horizontal:	lbs
Seismic Load Vertical:	psf

Step 7: Allowable Stress Design (ASD) Load Combinations (ASCE 7-10, Chapter 2, Section 2.4.1)

*The load combinations below have been identified as the likely controlling cases for the roof structure.

1) D

2) D + Lr

3) D + S

4) D + $0.6W_{up}$

5) D + $0.6W_{down}$

6) D + $0.75(0.6)W_{down} + 0.75S$

7) D + $0.75(0.6)W_{down}$ + 0.75Lr

8) D + 0.75(0.7E) + 0.75Lr

9) D + 0.75(0.7E) + 0.75S

10) D + 0.7E

11) $0.6D + 0.6W_{up}$

12) $0.6 D + 0.6W_{down}$

13) 0.6 D + 0.7E

D = Dead Load

Lr = Live Load to Roof

S = Snow Load

 W_{up} = Wind Load Up

 W_{down} = Wind Load Down

E = Earthquake/Seismic Load

Step 8: Create Initial Array Layout

- a. Identify the structural supporting members of your building. A sketch/drawing of the roof/building with location of supporting members, vents, skylights, cable/wires, areas to avoid, etc., is highly recommended.
- b. Create a "rough draft" layout of solar modules on the actual project roof. (Refer to the SOLARMOUNT Installation Guide.)



Step 9: Determine a Rail Span

*For structural engineers who would like to determine the rail span without utilizing the Prescriptive Method, section properties can be found in Appendix F - Technical Data Sheets.

- a. online.
- b. Use fill-in boxes below to document your project specific pressures and tables utilized.

Basic Wind Speed -	
Building Height -	
Exposure Category -	
Lateral (Ss) -	

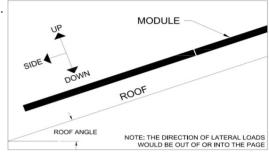
Roof Pitch

Ground Snow Load

Pressure Table Used:

Controlling Pressure:

	Up (psf)	Down (psf)	Side (psf)	Lateral (psf)
Roof zone 1:				
Roof zone 2:				
Roof zone 3:				
	Nota: For La	w Drofile Ma	da whara rai	la ara narna



Note: For Low Profile Mode, where rails are perpendicular to the roof tilt (E-W Rails), "Side Load" (Down Slope) is load applied in weak axis bending of the SOLARMOUNT rail along the roof tilt and "Lateral" is load applied as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt. For High Profile Mode, where rails are parallel to the roof tilt (N-S Rails), "Side Load" (Downslope) is load applied in as an axial load along the SOLARMOUNT rail perpendicular to the roof tilt and "Lateral Load" is applied in weak axis bending of the SOLARMOUNT rail along the roof tilt.

- c. Convert pressures (lbs/ft² or psf) from the boxes just filled in to pounds per linear foot (lb/ft or plf) using the following steps:
 - i. Pressure (from table above) * Area of Module = Total Pounds per Module
 - ii. Total Pounds Per Module / 2 (Number of rails) = Pounds Per Rail
 - iii. Pounds Per Rail / Width of Module Parallel with the Rail = Pounds per Linear Foot (plf)
- d. Use the Downward and Upward Span Length Tables in Appendix C with the plf loads to determine maximum spans.
 - Using the pir loads for "Down", look up the table "Downward Span Lengths" in the Appendix and
 - using the "Down" plf load and the "Side" plf load combinations to choose the maximum span length.
 - ii. Using the plf loads for "Up", look up the table "Uplift Span Lengths" in the Appendix and using the "Up" plf and "Side" plf load combinations to choose the maximum span length.
 - iii. Use the smaller length of the "Down" and "Up" maximum span length.
 - iv. Cantilever (overhang) lengths can be up to 33% of the span length. For example, a 9 foot span length can have a 3 foot cantilever. The cantilever is defined as the distance from the center of a L-Foot to the edge of a rail.



Step 10: Look-up Layout and Attachment Guidelines for Array

a. Review your layout in Step 8 above and the Layout and Attachment Guidelines to determine potential attachment points to your structure.

Step 11: Determine Load to the Roof

- a. To determine the load on the roof through the attachment:
 - i. Determine the tributary area to each attachment.
 - ii. Review the controlling pressure in Step 9.
 - iii. Determine pressure zones on the roof per ASCE 7-10, Figure 30.5-1.
 - iv. Multiply the tributary area by the roof pressure to obtain loads to the roof attachment.
 - v. Determine the point load to the roof at each attachment.

Step 12: Check Roof Load

a. Ensure that the supporting structure is capable of withstanding the additional loads imposed by the proposed solar system.

Step 13: Check the Connections

- a. Similar to Step 9c, determine the tributary area to each connection and the applied load from the Controlling Pressures table in Step 9
- b. Convert the applied psf loads into pounds through tributary area.
- c. Look up the Technical Data Sheets in Appendix G for maximum permissible load to each connection.
- d. From Step 11, determine if the attachment (lag bolt or other appropriate attachment) is capable of withstanding the point loads applied
- e. If the maximum permissible load is greater than the applied load, then the connections are adequate.

Step 14: Define Grounding and Bonding Path

a. Refer to the SOLARMOUNT Installation Guide for how to determine the Grounding and Bonding Path.

Step 15: SOLARMOUNT Front Trim Check

a. SOLARMOUNT Front Trim should not be installed in areas where the wind load exceeds 100 psf, where the distance from clamp to clamp (span) exceeds 52 inches, or where the cantilever (overhang) is greater than 66% of the span length. Please review the Step 6 Up and Down Wind Loads (psf) to determine if Front Trim is appropriate for your project.



Technical Support

If you have further questions regarding the SOLARMOUNT product, please contact your distributer. If further clarification is needed, please review the Unirac website online resources at:

http://unirac.com/solarmount

The Unirac website contains up-to-date manuals, design guides, webinars, online calculations, information, certification letters, technical data sheets, additional products that Unirac provides, and anything else you might need for your project.



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Appendix – Table of Contents

Appendix A – Product Catalog of Parts List
Appendix B – Pressure Lookup Tables
Appendix C – Downward & Upward Span Length Tables
Appendix D – Roof Pitch to Angle
Appendix E – Dead Load Analysis
Appendix F – Enphase Energy Microinverter Testing
Appendix G – Technical Data
Appendix H – SM HD Rail
Appendix I – Thermal Expansion





Please refer to the **Master Price List** at www.unirac.com for a list of part numbers, part descriptions, and prices.



Side Load (psf)

7-05 ASCE

California (Typical)*

85 mph

5 psf

Basic Wind Speed

Ground Snow Load

Up and Down (psf)

		8 9	Bldg. Height = 15	= 15	ft. Down	8	Bldg. Height = 30 ft.	ht = 30	ft.	B	Bldg. Height = 60	= 60	ft. Down
T	Roof Pitch	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(bst)
	1:12	9.6-	-18.4	-29.4	14.7	9.6-	-18.4	-29.4	14.7	-12.0	-22.7	-36.0	14.7
F	2:12	-8.6	-17.4	-27.3	14.3	9.8-	-17.4	-27.3	14.3	-10.7	-21.4	-33.4	14.3
-xp	3:12	-8.7	-17.4	-27.3	13.9	-8.7	-17.4	-27.3	13.9	-10.7	-21.4	-33.4	13.9
000	4:12	-8.7	-17.4	-27.3	13.5	-8.7	-17.4	-27.3	13.5	-10.7	-21.4	-33.4	13.5
ura	5:12	-8.7	-17.4	-27.3	13.2	-8.7	-17.4	-27.3	13.2	-10.8	-21.4	-33.5	13.2
	6:12	œ. œ.	-17.5	-27.4	13.1	-8.8	-17.5	-27.4	13.1	-10.8	-21.5	-33.5	13.1
`at	7:12	8.6-	-12.0	-12.0	13.0	-9.8	-12.0	-12.0	13.0	-12.2	-14.8	-14.8	15.0
200	8:12	6.6-	-12.1	-12.1	12.9	6.6-	-12.1	-12.1	12.9	-12.2	-14.9	-14.9	14.9
orv	9:12	6.6-	-12.1	-12.1	12.8	6.6-	-12.1	-12.1	12.8	-12.3	-14.9	-14.9	14.8
, B	10:12	6.6-	-12.1	-12.1	12.7	6.6-	-12.1	-12.1	12.7	-12.3	-15.0	-15.0	14.7
	11:12	-10.0	-12.2	-12.2	12.6	-10.0	-12.2	-12.2	12.6	-12.3	-15.0	-15.0	14.6
	12:12	-10.0	-12.2	-12.2	12.5	-10.0	-12.2	-12.2	12.5	-12.4	-15.1	-15.1	14.5
Ī	1.12	-120	7 66-	-36.0	14.7	-14.0	-26.4	418	14.7	-164	-30.6	-48.4	14.7
	2.12	107	21.4	20.00	14.5	12 5	24.0	20.7	14.5	146	2000	0 77	14.2
Ex	3.12	10.7	-21.4	-33.4	12.0	-12.5	-24.0	138.7	120	-14.7	-20.0	44.0	120
-	3.12	101	21.4	1.00	10.0	10.51	0.42	2000	10.0	147	20.00	44.0	10.0
	4:12	100	21.4	4.00-	13.3	12.0	24.5	0.00	13.3	14.7	20.07	44.0	10.0
-	2.12	100	21 5	300	10.1	12.6	0 30	0.00	10.1	140	20.00	AE 0	10.4
0	21.7	12.2	14.0	14.0	13.1	14.2	0.62-	17.0	13.1	-14.0	20.62	20.0	13.1
+-	7117	2.21-	-14.0	0.41-	13.0	-14.2	5.71-	-17.5	10.9	-10.0	1.02-	1.02-	13.0
	8:12	777-	-14.9	-14.9	14.9	-14.3	-17.3	-17.3	16.8	-10.0	2002	7.07-	18.9
	9:12	12.3	-14.9	-14.9	14.8	-14.3	47.4	17.4	10.7	-16.7	20.7	20.7	18.8
	10:12	-12.3	12.0	0.61-	14.7	+7+7+	47.7	47.74	10.0	-10.7	-20.3	-20.3	10.7
	11:12	-12.3	-15.0	-15.0	14.6	-14.4	-1/.5	-17.5	16.4	-16.8	-20.3	-20.3	18.6
T	12:12	-12.4	-15.1	-15.1	14.5	-14.4	-17.5	-17.5	16.3	-16.8	-20.3	-20.3	18.5
_	1:12	-14.8	-27.8	-44.0	14.7	-16.9	-31.5	-49.7	14.7	-19.2	-35.7	-56.3	14.7
_	2:12	-13.2	-26.2	-40.7	14.3	-15.1	-29.6	-46.1	14.3	-17.2	-33.7	-52.2	14.6
	3:12	-13.2	-26.2	-40.8	13.9	-15.1	-29.7	-46.1	13.9	-17.2	-33.7	-52.2	14.2
-	4:12	-13.3	-26.2	-40.8	13.5	-15.1	-29.7	-46.1	13.5	-17.2	-33.7	-52.2	13.7
	5:12	-13.3	-26.3	-40.8	13.2	-15.1	-29.7	-46.1	13.2	-17.3	-33.7		13.5
C	6:12	-13.3	-26.3	-40.9	13.1	-15.2	-29.8	-46.2	13.1	-17.3	-33.8	-52.3	13.4
- 1	7:12	-12.0	-18.2	-18.2	17.6	-17.0	-20.7	-20.7	19.4	-19.4	-23.5	-23.5	21.6
	8:12	-15.0	-18.3	-18.3	17.5	-17.1	-20.7	-20.7	19.3	-19.5		-23.6	21.4
	9:12	-15.1	-18.3	-18.3	17.4	-17.1	-20.8	-20.8	19.2	-19.5	-23.6	-23.6	21.3
	10:12	-15.1	-18.4	-18.4	17.3	-17.2	-20.8	-20.8	19.1	-19.5	-23.7	-23.7	21.2
	11:12	-15.2	-18.4	-18.4	17.2		-20.9	-20.9	19.0	-19.6	-23.7	-23.7	21.1
\neg	12:12	-15.2	-18.5	-18.5	17.0	-17.3	-20.9	-20.9	18.9	-19.6	-23.7	-23.7	21.0
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	$S_{S} = 0.5$	$S_S = 1.0$	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
_	1:12	0.7	8.0	6.0	1.1	1.2	1.3	1.8	2.0	2.3	2.9	3.6	4.4
	2:12	1.3	1.3	1.5	1.6	1.7	1.9	2.3	2.4	2.7	3.3	3.9	4.7
_	3:12	1.9	1.9	5.0		2.2				3.1	3.7	4.2	
	4:12	2.4	2.4	2.4	2.5	5.6	2.8	3.2	3.3	3.6	4.1	4.6	5.3
	5:12	2.7	2.7	2.7	2.9	3.0	3.1	3.5	3.6	3.9	4.4	4.9	5.5
- 0	6:12	3.1	3.1	3.1	3.1	3.3	3.4	3.8	3.9	4.2	4.7	5.1	5.7
lop	7:12	3.3	3.3	3.3	3.4	3.5	3.6	4.0	4.1	4.4	4.9	5.3	5.9
	8:12	3.5	3.5	3.5	3.5	3.7	3.8	4.1	4.3	4.5	2.0	5.5	0.9
	9:12	3.6	3.6	3.6	3.7	3,8	3.9	4.3	4.4	4.6	5.1	9.9	6.1
	10:12	3.7	3.7	3.7	3.8	3.9	4.0	4.4	4.5	4.7	5.2	2.6	6.2
	11:12	w 6		w o	9.6	4.0	4.1		4.5	8. 4	5.2	5.7	6.2
\dashv	12:12	3.8	3.8	3.8	3.9	4.0	4.1	4.4	4.6	4.8	5.2	5.7	6.2
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss	Ss = 2.0	Ss = 2.5	Ss = 3.1
		0.0	0.2	0.4	9.0	0.8	0.9	1.4	1.6	2.0	2.6	3.3	4.0

Lateral



Southwest (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

90 mph

5 psf

Basic Wind Speed

Ground Snow Load

		8 Å	Bldg. Height	= 15	ft. Down	8 d	Bldg. Height = 30 ft. Up pressures (psf)	ht = 30 f		8	Bldg. Height = 60 Uppressures (psf)	9 =	ft. Down	
	Roof Pitch	Zone 1	Zone 2		(bst)	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1		Zone 3	(Jsd)	
	1:12	-11.0	-20.8	-33.2	14.7	-11.0	-20.8	-33.2	14.7	-13.6	-25.6	-40.6	14.7	
Ex	3.12	۸. ۵	-19.6	-30.7	12.0	رن م م	19.6	-30.7	12.0	-12.1	-24.1	-37.6	12.0	
pos	4:12	8.6	-19.7	-30.8	13.5	8.0-	-19.7	-30.8	13.5	-12.2		-37.6	13.5	
sur	5:12	-9.8	-19.7	-30.8	13.2	8.6-	-19.7	-30.8	13.2	-12.2	-24.2	-37.7	13.2	
e C	6:12	-9.9	-19.7	-30.8	13.1	6.6-	-19.7	-30.8	13.1	-12.3	-24.2	-37.7	13.1	
Cat	7:12	-11.1	-13.6	-13.6	14.1	-11.1	-13.6	-13.6	14.1	-13.8	-16.8	-16.8	16.5	
eg	8:12	-11.2	-13.7	-13.7	14.0	-11.2	-13.7	-13.7	14.0	-13.8	-16.8	-16.8	16.4	
ory	9:12	-11.2	-13.7	-13.7	13.9	-11.2	-13.7	-13.7	13.9	-13.9	-16.9	-16.9	16.3	
В	10:12	-11.3	-13.7	-13.7	13.8	-11.3	-13.7	-13.7	13.8	-13.9	-16.9	-16.9	16.2	
	11:12	-11.3	-13.8	-13.8	13.7	-11.3	-13.8	-13.8	13.7	-14.0	-17.0	-17.0	16.1	
	12:12	-11.4	-13.8	-13.8	13.6	-11.4	-13.8	-13.8	13.6	-14.0	-17.0	-17.0	16.0	
	1:12	-13.6	-25.6	-40.6	14.7	-15.9	-29.7	-47.0	14.7	-18.5	-34.5	-54.4	14.7	
-	2:12	-12.1	-24.1	-37.6	14.3	-14.2	-28.0	-43.6	14.3	-16.6		-50.4	14.3	
Exp	3:12	-12.1	-24.1	-37.6	13.9	-14.2	-28.0	-43.6	13.9	-16.6	-32.5	-50.4	13.9	
008	4:12	-12.2	-24.2	-37.6	13.5	-14.2	-28.1	-43.6	13.5	-16.6	-32.6	-50.5	13.5	
sure	5:12	-12.2	-24.2	-37.7	13.2	-14.3	-28.1	-43.6	13.2	-16.7	-32.6	-50.5	13.2	
e C	6:12	-12.3	-24.2	-37.7	13.1	-14.3	-28.1	-43.7	13.1	-16.7	-32.6	-50.6	13.1	
Cat	7:12	-13.8	-16.8	-16.8	16.5	-16.1	-19.5	-19.5	18.6	-18.7	-22.7	-22.7	20.9	
eg	8:12	-13.8	-16.8	-16.8	16.4	-16.1	-19.6	-19.6	18.5	-18.8	-22.8	-22.8	20.8	
ory	9:12	-13.9	-16.9	-16.9	16.3	-16.2	-19.6	-19.6	18.3	-18.8	-22.8	-22.8	20.7	
y C	10:12	-13.9	-16.9	-16.9	16.2	-16.2	-19.7	-19.7	18.2	-18.9	-22.8	-22.8	20.6	
)	11:12	-14.0	-17.0	-17.0	16.1	-16.3	-19.7	-19.7	18.1	-18.9	-22.9	-22.9	20.5	
	12:12	-14.0	-17.0	-17.0	16.0	-16.3	-19.8	-19.8	18.0	-18.9		-22.9	20.4	
	,	,		Ş	;	Ş	,		;		9	6	;	
	1:12	-16.8	-31.3	-49.5	14.7	-19.1	-35.4	-55.9	14.7	-21.7	-40.2	-63.3	14.7	
Е	2:12	-15.0	-29.5	-45.8	14.3	-17.0	-33.4	-51.8	14.5	-19.4	-37.9	-58.7	15.5	
хр	3:12	-15.0	-29.5	-45.9	13.9	-17.1	-33.4	-51.8	14.1	-19.4	-37.9	-58.7	15.1	
osı	4:12	-15.0	-29.6	-45.9	13.5	-17.1	-33.5	-51.9	13.7	-19.5	-37.9	-58.7	14.9	
ure	5:12	-15.1	-29.6	-45.9	13.2	-17.1	-33.5	-51.9	13.5	-19.5	-38.0	-58.8	14.8	
C	6:12	-15.1	-29.6	-46.0	13.1	-17.2	-33.5	-51.9	13.4	-19.6	-38.0	-58.8	14.7	
ate	7:12	-17.0	-20.6	-20.6	19.4	-19.3	-23.3	-23.3	21.4	-21.9	-26.5	-26.5	23.8	
eg	8:12	-17.0	-20.6	-20.6	19.2	-19.3	-23.4	-23.4	21.3	-21.9	-26.6	-26.6	23.7	
ory	9:12	-17.1	-20.7	-20.7	19.1	-19.3	-23.4	-23.4	21.2	-22.0	-26.6	-26.6	23.6	
D	10:12	-17.1	-20.7	-20.7	19.0	-19.4	-23.5	-23.5	21.1	-22.0	-26.7	-26.7	23.5	
	11:12	-17.1	-20.8	-20.8		-19.4	-23.5		21.0	-22.1	-26.7		23.4	
	12:12	-17.2	-20.8	-20.8	18.8	-19.5	-23.6	-23.6	20.9	-22.1	-26.7	-26.7	23.3	
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1	
	1:12	0.7	0.8	6.0	1.1	1.2	1.3	1.8	2.0	2.3	2.9	3.6	4.4	
	2:12	1.3	1.3	1.5	1.6	1.7	1.9	2.3	2.4	2.7	3.3	3.9	4.7	
	3:12	1.9	1.9	2.0	2.1	2.2	2.3		2.9	3.1	3.7	4.2	5.0	
Do	4:12	2.4	2.4	2.4	2.5	5.6	2.8	3.2	3.3	3.6	4.1	4.6	5.3	
ow	5:12	2.7	2.7	2.7	2.9	3.0	3.1	3.5	3.6	3.9	4.4	4.9	5.5	
n S	6:12	3.1	3.1	3.1	3.1	3.3	3.4	3.8		4.2	4.7	5.1	5.7	
Slo	7:12	3.3	3.3	3.3	3.4	3.5	3.6	4.0		4.4	4.9	5.3	5.9	
ре	8:12	3.5	3.5	3.5	3.5	3.7	3.8	4.1	4.3	4.5	5.0	5.5	6.0	
	9:12	3.6	3.6	3.6	3.7	3.8	3.9	4.3	4.4	4.6	5.1	5.6	6.1	
	10:12	3.7	3.7	3.7	3.8	3.9	4.0	4.4	4.5	4.7	5.2	5.6	6.2	
	11:12	3.8	3.8	3.8	3.9	4.0	4.1	4.4	4.5	4.8	5.2	5.7	6.2	
	12:12	3.8	3.8	3.8	3.9	4.0	4.1	4.4	4.6	4.8	5.2	5.7	6.2	
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1	
		0			(0	•	;	•			•		

Up and Down (psf)

Side Load (psf)

Lateral



Mid US (Medium Snow)*

90 mph

25 psf

Basic Wind Speed

Ground Snow Load

		8	Bldg. Height	Bldg. Height = 15 ft		BI dn	Bldg. Height	Bldg. Height = 30 ft.	t. Down	B	Bldg. Height = 60	9 =	ft. Down
	Roof Pitch	Zone 1	Zone 2		(bst)	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)
	1:12	-11.0	-20.8	-33.2	25.9	-11.0	-20.8	-33.2	25.9	-13.6	-25.6	-40.6	25.9
E	2:12	-9.7	-19.6	-30.7	24.5	-9.7	-19.6	-30.7	24.5	-12.1	-24.1	-37.6	24.5
хр	3:12	8.6-	-19.6	-30.7	23.0	8.6-	-19.6	-30.7	23.0	-12.1	-24.1	-37.6	23.0
os	4:12	-9.8	-19.7	-30.8	21.5	-9.8	-19.7	-30.8	21.5	-12.2	-24.2	-37.6	21.5
ure	5:12	-9.8	-19.7	-30.8	20.0	-9.8	-19.7	-30.8	20.0	-12.2	-24.2	-37.7	20.0
C	6:12	6.6-	-19.7	-30.8	18.6	6.6-	-19.7	-30.8	18.6	-12.3	-24.2	-37.7	18.6
ate	7:12	-11.1	-13.6	-13.6	18.2	-11.1	-13.6	-13.6	18.2	-13.8	-16.8	-16.8	20.0
eg	8:12	-11.2	-13.7	-13.7	17.0	-11.2	-13.7	-13.7	17.0	-13.8	-16.8	-16.8	18.8
ory	9:12	-11.2	-13.7	-13.7	16.0	-11.2	-13.7	-13.7	16.0	-13.9	-16.9	-16.9	17.8
/В	10:12	-11.3	-13.7	-13.7	15.1	-11.3	-13.7	-13.7	15.1	-13.9	-16.9	-16.9	16.9
	11:12	-11.3	-13.8	-13.8	14.4	-11.3	-13.8	-13.8	14.4	-14.0	-17.0	-17.0	16.1
	12:12	-11.4	-13.8	-13.8	13.7	-11.4	-13.8	-13.8	13.7	-14.0	-17.0	-17.0	16.0
	1:12	-13.6	-25.6	-40.6	25.9	-15.9	-29.7	-47.0	25.9	-18.5	-34.5	-54.4	25.9
	2:12	-12.1	-24.1	-37.6	24.5	-14.2	-28.0	-43.6	24.5	-16.6	-32.5	-50.4	24.5
Ex	3:12	-12.1	-24.1	-37.6	23.0	-14.2	-28.0	-43.6	23.0	-16.6		-50.4	23.0
00	4:12	-12.2	-24.2	-37.6	21.5	-14.2	-28.1	-43.6	21.5	-16.6		-50.5	21.5
sur	5:12	-12.2	-24.2	-37.7	20.0	-14.3	-28.1	-43.6	20.0	-16.7		-50.5	20.0
е	6:12	-12.3	-24.2	-37.7	18.6	-14.3	-28.1	-43.7	18.6	-16.7		-50.6	18.6
Ca	7:12	-13.8	-16.8	-16.8	20.0	-16.1	-19.5	-19.5	21.5	-187	-22.7	-22.7	23.3
teg	8:12	-13.8	-16.8	-16.8	18.8	-16.1	-19.6	-19.6	20.4	-18.8		-22.8	22.2
jor	0.10	12.0	16.0	16.0	17.0	16.2	10.6	10.6	107	200	22.22	22.0	21.1
у (10.12	100	16.0	10.01	10.0	10.7	10.7	10.7	10.4	10.0	33.0	0.22-	200
С	10:12	-13.9	-10.9	E.O.T.	10.9	7.01-	1.61-	-13./	18.0	-10.9	977-	27.7	20.0
	11:12	-14.0	-17.0	-17.0	16.1	-16.3	-19.7	-19.7	18.1	-18.9	-22.9	-22.9	20.5
	12:12	-14.0	-17.0	-17.0	16.0	-16.3	-19.8	-19.8	18.0	-18.9	-22.9	-22.9	20.4
	1:12	-16.8	-31.3	-49.5	25.9	-19.1	-35.4	-55.9	25.9	-21.7	-40.2	-63.3	25.9
E	2:12	-15.0	-29.5	-45.8	24.5	-17.0	-33.4	-51.8	24.7	-19.4	-37.9	-58.7	25.7
Хþ	3:12	-15.0	-29.5	-45.9	23.0	-17.1	-33.4	-51.8	23.2	-19.4	-37.9	-58.7	24.2
os	4:12	-15.0	-29.6	-45.9	21.5	-17.1	-33.5	-51.9	21.7	-19.5	-37.9	-58.7	22.7
sur	5:12	-15.1	-29.6	-45.9	20.0	-17.1	-33.5	-51.9	20.2	-19.5	-38.0	-58.8	21.2
e (6:12	-15.1	-29.6	-46.0	18.6	-17.2	-33.5	-51.9	18.8	-19.6	-38.0	-58.8	19.8
Cat	7:12	-17.0	-20.6	-20.6	22.1	-19.3	-23.3	-23.3	23.7	-21.9	-26.5	-26.5	25.4
eg	8:12	-17.0	-20.6	-20.6	21.0	-19.3	-23.4	-23.4	22.5	-21.9	-26.6	-26.6	24.3
ory	9:12	-17.1	-20.7	-20.7	19.9	-19.3	-23.4	-23.4	21.5	-22.0	-26.6	-26.6	23.6
/ D	10:12	-17.1	-20.7	-20.7	19.1	-19.4	-23.5	-23.5	21.1	-22.0	-26.7	-26.7	23.5
	11:12	-17.1	-20.8	-20.8	18.9	-19.4	-23.5	-23.5	21.0	-22.1	-26.7	-26.7	23.4
	12:12	-17.2	-20.8	-20.8	18.8	-19.5	-23.6	-23.6	20.9	-22.1	-26.7	-26.7	23.3
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	2.0	2.0	2.0	2.0	2.1	2.2	5.6	2.8	3.0	3.5	4.0	4.6
	2:12	3.6	3.6	3.6	3.6	3.6	3.6	4.0	4.1	4.4	4.9	5.4	6.0
	3:12	5.0	5.0	5.0	5.0	5.0	5.0	5.1	5.2	5.5	6.0	6.5	7.1
Do	4:12	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.4	6.9	7.4	8.0
ow	5:12	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.5	8.0	8.6
n S	6:12	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	8.0	8.5	9.1
Slo	7:12	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	8.3	89.	9.4
pe	8:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.5	9.0	9.5
	9:12	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.5	9.0	9.6
	10:12	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.5	0.6	9.5
	11:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.4	8.9	9.4
	12:12	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	8.3	8.7	9.2
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
		0	0	*	0	0	c	,		0	0	•	

Lateral

0.8

9.0

0.2



7.05 ASCE

Massachusetts (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

90 mph

40 psf

Basic Wind Speed

Ground Snow Load

		<u>8</u> 9	Bldg. Height = 15	= 15	ft.	<u>8</u>	Bldg. Height = 30 ft.	tht = 30	ft.	8 9	Bldg. Height =	9 =	ft.
T	Roof Pitch	Zone 1	Zone 2	Zone 3	(pst)	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bsd)
	1:12	-11.0	-20.8	-33.2	31.8	-11.0	-20.8	-33.2	31.8	-13.6	-25.6	-40.6	31.8
E	2:12	-9.7	-19.6	-30.7	30.0	-9.7	-19.6	-30.7	30.0	-12.1	-24.1	-37.6	30.0
xp	3:12	-9.8	-19.6	-30.7	27.9	8.6-	-19.6	-30.7	27.9	-12.1	-24.1	-37.6	27.9
os	4:12	-9.8	-19.7	-30.8	25.8	8.6-	-19.7	-30.8	25.8	-12.2	-24.2	-37.6	25.8
ure	5:12	-9.8	-19.7	-30.8	23.8	8.6-	-19.7	-30.8	23.8	-12.2	-24.2	-37.7	23.8
e C	6:12	-9.9	-19.7	-30.8	21.9	6.6-	-19.7	-30.8	21.9	-12.3	-24.2	-37.7	21.9
at	7:12	-11.1	-13.6	-13.6	20.9	-11.1	-13.6	-13.6	20.9	-13.8	-16.8	-16.8	22.7
eg	8:12	-11.2	-13.7	-13.7	19.4	-11.2	-13.7	-13.7	19.4	-13.8	-16.8	-16.8	21.1
ory	9:12	-11.2	-13.7	-13.7	18.0	-11.2	-13.7	-13.7	18.0	-13.9	-16.9	-16.9	19.8
/ B	10:12	-11.3	-13.7	-13.7	16.8	-11.3	-13.7	-13.7	16.8	-13.9	-16.9	-16.9	18.6
	11:12	-11.3	-13.8	-13.8	15.7	-11.3	-13.8	-13.8	15.7	-14.0	-17.0	-17.0	17.5
	12:12	-11.4	-13.8	-13.8	14.8	-11.4	-13.8	-13.8	14.8	-14.0	-17.0	-17.0	16.6
	1:12	-13.6	-25.6	-40.6	31.8	-15.9	-29.7	-47.0	31.8	-18.5	-34.5	-54.4	31.8
	2:12	-12.1	-24.1	-37.6	30.0	-14.2	-28.0	-43.6	30.0	-16.6	-32.5	-50.4	30.0
Exp	3:12	-12.1	-24.1		27.9	-14.2	-28.0	-43.6	27.9	-16.6		-50.4	27.9
00:	4:12	-12.2	-24.2	-37.6	25.8	-14.2	-28.1	-43.6	25.8	-16.6	-32.6	-50.5	25.8
sur	5:12	-12.2	-24.2	-37.7	23.8	-14.3	-28.1	-43.6	23.8	-16.7	-32.6	-50.5	23.8
e (6:12	-12.3	-24.2	-37.7	21.9	-14.3	-28.1	-43.7	21.9	-16.7	-32.6	-50.6	21.9
Cat	7:12	-13.8	-16.8	-16.8	22.7	-16.1	-19.5	-19.5	24.3	-18.7	-22.7	-22.7	26.0
eg	8:12	-13.8	-16.8	-16.8	21.1	-16.1	-19.6	-19.6	22.7	-18.8	-22.8	-22.8	24.5
orv	9:12	-13.9	-16.9	-16.9	19.8	-16.2	-19.6	-19.6	21.3	-18.8	-22.8	-22.8	23.1
/ C	10:12	-13.9	-16.9	-16.9	18.6	-16.2	-19.7	-19.7	20.1	-18.9	-22.8	-22.8	21.9
,	11:12	-14.0	-17.0	-17.0	17.5	-16.3	-19.7	-19.7	19.1	-18.9	-22.9	-22.9	20.8
	12:12	-14.0	-17.0	-17.0	16.6	-16.3	-19.8	-19.8	18.2	-18.9	-22.9	-22.9	20.4
Ī	1.12	-16.8	-313	-49 5	29.8	-191	-35.4	-55.0	29.8	-217	-40.2	-63.3	29.8
	2:12	-15.0	-29.5	-45.8	28.1	-17.0	-33.4	-51.8	28.2	-19.4	-37.9	-58.7	29.2
Ex	2.12	100	200	AF 0	26.2	17.1	22.4	1010	207	10.4	27.0	7.00	27.7
po	3.12	-15.0	20.6	-45.9	20.2	-17.1	-32.5	510	24.5	-19.4	27.0	-58.7	25.5
su	5.12	15.1	20.6	45.0	22.5	17.1	22.5	210	22.6	10.5	38.0	000	22.6
re	6:12	-15.1	-29.6	-46.0	20.7	-17.2	-33.5	-519	20.9	-19.6	-38.0	2000	21.0
Ca	7:12	-17.0	-20.6	-20.6	23.9	-19.3	-23.3	-23.3	25.4	-21.9	-26.5	-26.5	27.2
teg	8:12	-17.0	-20.6	-20.6	22.5	-19.3	-23.4	-23.4	24.0	-21.9	-26.6	-26.6	25.8
ory	9:12	-17.1	-20.7	-20.7	21.2	-19.3	-23.4	-23.4	22.8	-22.0	-26.6	-26.6	24.5
/ D	10:12	-17.1	-20.7	-20.7	20.1	-19.4	-23.5	-23.5	21.7	-22.0	-26.7	-26.7	23.5
	11:12	-17.1	-20.8	-20.8	19.2	-19.4	-23.5	-23.5	21.0	-22.1	-26.7	-26.7	23.4
	12:12	-17.2	-20.8	-20.8	18.8	-19.5	-23.6	-23.6	20.9	-22.1	-26.7	-26.7	23.3
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	5.6	5.6	5.6	2.6	5.6	2.7	3.1	3.3	3.5	4.0	4.5	5.1
	2:12	4.9	4.9	4.9	4.9	4.9	4.9	4.9	5.0	5.3	5.8	6.3	6.9
	3:12	6.7	6.7	6.7	6.7	6.7	6.7	6.7	6.7	6.7	7.3	7.8	8.4
Do	4:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.4	8.9	9.5
wr	5:12	9.5	9.2	9.2	9.2	9.2	9.2	9.2	9.5	9.2	9.2	9.7	10.3
ı S	6:12	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	10.3	10.9
lop	7:12	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.7	11.2
е	8:12	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.8	11.4
	9:12	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.8	11.4
	10:12	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.6	10.8	11.3
	11:12	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.6	11.1
	12:12	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.3	10.9
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1

Lateral

0.9

0.8

9.0

0.4

0.2



Mid US (High Snow)*

90 mph

60 psf

Basic Wind Speed

Ground Snow Load

Up and Down (psf)

		a y	Bldg. Height = 15 Up Pressures (psf)	= 15	ft. Down	8 d	Bldg. Height = 30 ft.	ht = 30 i		B d	Bldg. Height = 60 Uppressures (psf)	= 60	ft. Down
T	Roof Pitch	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)
	1:12	-11.0	-20.8	-33.2	45.2	-11.0	-20.8	-33.2	45.2	-13.6	-25.6	-40.6	45.2
F	2:12	-9.7	-19.6	-30.7	41.5	-9.7	-19.6	-30.7	41.5	-12.1	-24.1	-37.6	41.5
vn	3:12	-9.8	-19.6	-30.7	37.4	8.6-	-19.6	-30.7	37.4	-12.1	-24.1	-37.6	37.4
000	4:12	-9.8	-19.7	-30.8	33.3	8.6-	-19.7	-30.8	33.3	-12.2	-24.2	-37.6	33.3
1154	5:12	-9.8	-19.7	-30.8	30.3	8.6-	-19.7	-30.8	30.3	-12.2	-24.2	-37.7	30.3
- (6:12	-9.9	-19.7	-30.8	27.5	6.6-	-19.7	-30.8	27.5	-12.3	-24.2	-37.7	27.5
at	7:12	-11.1	-13.6	-13.6	25.7	-11.1	-13.6	-13.6	25.7	-13.8	-16.8	-16.8	27.5
eg	8:12	-11.2	-13.7	-13.7	23.4	-11.2	-13.7	-13.7	23.4	-13.8	-16.8	-16.8	25.2
Orv	9:12	-11.2	-13.7	-13.7	21.4	-11.2	-13.7	-13.7	21.4	-13.9	-16.9	-16.9	23.2
, B	10:12	-11.3	-13.7	-13.7	19.7	-11.3	-13.7	-13.7	19.7	-13.9	-16.9	-16.9	21.4
	11:12	-11.3	-13.8	-13.8	18.1	-11.3	-13.8	-13.8	18.1	-14.0	-17.0	-17.0	19.9
	12:12	-11.4	-13.8	-13.8	16.9	-11.4	-13.8	-13.8	16.9	-14.0	-17.0	-17.0	18.6
Г	1:12	-13.6	-25.6	-40.6	45.2	-15.9	-29.7	-47.0	45.2	-18.5	-34.5	-54.4	45.2
	2.12	-121	-24.1	-376	41.5	-14.2	-28.0	-43.6	41.5	-166	-37 5	-50.4	415
Ev	21.7	131	24.4	0.76	07.4	14.2	0.02	43.0	0.14	10.0	22.3	1.00	27.4
no	3.12	1.21-	1.42-	0.75-	4.70	7.4.7	0.02-	0.04	4.70	-10.0	5.25-	4.00-	4.70
วรน	4:12	12.2	7.47-	-3/.6	33.3	-14.2	1.82-	43.6	33.3	-16.6	-32.6	50.5	33.3
	5:12	-17.7	7.47-	-3/./	30.3	-14.3	1.82-	43.0	30.3	-Tp./	-32.6	-50.5	30.3
0	6:12	-12.3	-24.2	-37.7	27.5	-14.3	-28.1	-43.7	27.5	-16.7	-32.6	-50.6	27.5
	7:12	-13.8	-16.8	-16.8	27.5	-16.1	-19.5	-19.5	29.1	-18.7	-22.7	-22.7	30.8
	8:12	-13.8	-16.8	-16.8	25.2	-16.1	-19.6	-19.6	26.8	-18.8	-22.8	-22.8	28.5
	9:12	-13.9	-16.9	-16.9	23.2	-16.2	-19.6	-19.6	24.7	-18.8	-22.8	-22.8	26.5
_	10:12	-13.9	-16.9	-16.9	21.4	-16.2	-19.7	-19.7	23.0	-18.9	-22.8	-22.8	24.8
	11:12	-14.0	-17.0	-17.0	19.9	-16.3	-19.7	-19.7	21.5	-18.9	-22.9	-22.9	23.3
	12:12	-14.0	-17.0	-17.0	18.6	-16.3	-19.8	-19.8	20.2	-18.9	-22.9	-22.9	22.0
	1:12	-16.8	-31.3	-49.5	41.0	-19.1	-35.4	-55.9	41.0	-21.7	-40.2	-63.3	41.0
_	2:12	-15.0	-29.5	-45.8	37.7	-17.0	-33.4	-51.8	37.7	-19.4	-37.9	-58.7	37.8
	3:12	-15.0	-29.5	-45.9	34.0	-17.1	-33.4	-51.8	34.0	-19.4	-37.9	-58.7	35.0
	4:12	-15.0	-29.6	-45.9	31.1	-17.1	-33.5	-51.9	31.2	-19.5	-37.9	-58.7	32.2
	5:12	-15.1	-29.6	-45.9	28.3	-17.1	-33.5	-51.9	28.5	-19.5	-38.0	-58.8	29.5
	6:12	-15.1	-29.6	-46.0	25.8	-17.2	-33.5	-51.9	26.0	-19.6	-38.0	-58.8	26.9
	7:12	-17.0	-20.6	-20.6	28.2	-19.3	-23.3	-23.3	29.8	-21.9	-26.5	-26.5	31.5
	8:12	-17.0	-20.6	-20.6	26.1	-19.3	-23.4	-23.4	27.7	-21.9	-26.6	-26.6	29.5
ory	9:12	-17.1	-20.7	-20.7	24.3	-19.3	-23.4	-23.4	25.8	-22.0	-26.6	-26.6	27.6
-	10:12	-17.1	-20.7	-20.7	22.7	-19.4	-23.5	-23.5	24.3	-22.0	-26.7	-26.7	26.0
	11:12	-17.1	-20.8	-20.8	21.3	-19.4	-23.5	-23.5	22.9	-22.1	-26.7	-26.7	24.7
	12:12	-17.2	-20.8	-20.8	20.2	-19.5	-23.6	-23.6	21.7	-22.1	-26.7	-26.7	23.5
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	3.8	3.8	4.0	4.5	4.9	5.3	9.9	7.1	8.0	9.7	11.6	14.3
	2:12	7.0	7.0	7.0	7.0	7.3	7.7	9.0	9.5	10.3	11.9	13.5	15.5
	3:12	9.6	9.6	9.6	9.6	9.6	9.6	10.8	11.3	12.1	13.6	15.2	17.0
<u></u>	4:12	11.6	11.6	11.6	11.6	11.6	11.6	12.2	12.7	13.4	14.9	16.3	18.1
	5:12	13.1	13.1	13.1	13.1	13.1	13.1	13.2	13.6	14.3	15.7	17.0	18.7
	6:12	14.1	14.1	14.1	14.1	14.1	14.1	14.1	14.2	14.8	16.1	17.4	18.9
lop	7:12	14.7	14.7	14.7	14.7	14.7	14.7	14.7	14.7	15.1	16.3	17.4	18.9
	8:12	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0	16.2	17.3	18.6
	9:12	14.9	14.9	14.9	14.9	14.9	14.9	14.9	14.9	14.9	15.9	16.9	18.1
	10:12	14.7	14.7	14.7	14.7	14.7	14.7	14.7	14.7	14.7	15.5	16.4	17.6
	11:12	14.4	14.4	14.4	14.4	14.4	14.4	14.4	14.4	14.4	14.9	15.8	16.9
	12:12	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9		14.4	15.2	16.2
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1

Lateral

Side Load (psf)

0.0



East Coast (Medium Snow)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

100 mph

25 psf

Basic Wind Speed

Ground Snow Load

		6 5	Bidg. Height = 15 Jo Pressures (osf)	T T	Down	Up	Up Pressures (psf)	Jp Pressures (psf)	Down	Up Pressures (psf)	Up Pressures (psf)	(Jsc	Down
-	Roof Pitch	Zone 1	1 Zone 2 Zo	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(pst)
	1:12	-13.9	-26.0	-41.3	25.9	-13.9	-26.0	-41.3	25.9	-17.1	-31.9	-50.4	25.9
	2:12	-12.4	-24.5	-38.2	24.5	-12.4	-24.5	-38.2	24.5	-15.3	-30.1	-46.7	24.5
	3:12	-12.4	-24.6	-38.3	23.0	-12.4	-24.6	-38.3	23.0	-15.3	-30.1	-46.8	23.0
	4:12	-12.4	-24.6	-38.3	21.5	-12.4	-24.6	-38.3	21.5	-15.3	-30.1	-46.8	21.5
	5:12	-12.4	-24.6	-38.3	20.0	-12.4	-24.6	-38.3	20.0	-15.4	-30.2	-46.8	20.0
	6:12	-12.5	-24.7	-38.4	18.6	-12.5	-24.7	-38.4	18.6	-15.4	-30.2	-46.9	18.6
	7:12	-14.0	-17.1	-17.1	20.1	-14.0	-17.1	-17.1	20.1	-17.3	-21.0	-21.0	22.3
	8:12	-14.1	-17.1	-17.1	19.0	-14.1	-17.1	-17.1	19.0	-17.4	-21.1	-21.1	21.2
	9:12	-14.1	-17.2	-17.2	18.0	-14.1	-17.2	-17.2	18.0	-17.4	-21.1	-21.1	20.2
	10:12	-14.2	-17.2	-17.2	17.1	-14.2	-17.2	-17.2	17.1	-17.4	-21.1	-21.1	19.3
	11:12	-14.2	-17.3	-17.3	16.3	-14.2	-17.3	-17.3	16.3	-17.5	-21.2	-21.2	19.2
	12:12	-14.3	-17.3	-17.3	16.2	-14.3	-17.3	-17.3	16.2	-17.5	-21.2	-21.2	19.1
	1.12	171	21.0	E OZ	25.0	20.00	0.76	202	25.0	23.2	42.0	2 72	25.0
	77.7	11./1-	5.10-	4.00	5.03	0.02-	0.70	0.00-	6.03	7.67-	6.24-	6.70-	20.03
	71:7	-15.3	-30.1	-40./	24.5	-17.8	-34.9	-54.1	72.0	-20.8	-40.4	-62.b	70.3
- 1	3:12	-15.3	-30.1	-46.8	23.0	-17.9	-34.9	-54.1	23.5	-20.8	-40.5	-62.6	24.8
	4:12	-15.3	-30.1	-46.8	21.5	-17.9	-34.9	-54.1	22.0	-20.8	-40.5	-62.6	23.2
	5:12	-15.4	-30.2	-46.8	20.0	-17.9	-35.0	-54.2	20.5	-20.9	-40.5	-62.7	21.8
	6:12	-15.4	-30.2	-46.9	18.6	-18.0	-35.0	-54.2	19.1	-20.9	-40.6	-62.7	20.4
	7:12	-17.3	-21.0	-21.0	22.3	-20.1	-24.4	-24.4	24.3	-23.4	-28.3	-28.3	26.5
	8:12	-17.4	-21.1	-21.1	21.2	-20.2	-24.4	-24.4	23.1	-23.4	-28.4	-28.4	25.3
	9:12	-17.4	-21.1	-21.1	20.2	-20.2	-24.5	-24.5	22.1	-23.5	-28.4	-28.4	24.9
	10:12	-17.4	-21.1	-21.1	19.3	-20.3	-24.5	-24.5	21.9	-23.5	-28.4	-28.4	24.8
	11:12	-17.5	-21.2	-21.2	19.2	-203	-246	-246	21.8	-23.6	- 28.5	-28.5	747
	12.12	175	-212	21.2	101	-20.4	-246	-246	217	23.6	28.5	28.5	24 G
	12.12	C/T-	7.17-	7.77-	13.1	-20.4	0.42-	0.42-	7.77	-23.0	5.02-	C'07-	74.0
- 1	1:12	-21.0	-39.0	-61.4	25.9	-23.9	-44.1	-69.3	25.9	-27.1	-49.9	-78.4	25.9
	2:12	-18.8	-36.7	-56.9	25.4	-21.4	-41.6	-64.3	26.5	-24.3	-47.1	-72.8	27.7
	3:12	-18.8	-36.8	-56.9	24.0	-21.4	-41.6	-64.3	25.0	-24.3	-47.1	-72.8	26.2
	4:12	-18.9	-36.8	-57.0	22.4	-21.4	-41.6	-64.3	23.5	-24.4	-47.2	-72.8	24.7
1	5:12	-18.9	-36.8	-57.0	20.9	-21.4	-41.6	-64.4	22.0	-24.4	-47.2	-72.8	23.2
	6:12	-18.9	-36.9	-57.0	19.6	-21.5	-41.7	-64.4	20.6	-24.4	-47.2	-72.9	21.8
	7:12	-21.2	-25.7	-25.7	25.0	-24.1	-29.1	-29.1	26.9	-27.3	-33.0	-33.0	29.1
	8:12	-21.3	-25.8	-25.8	23.8	-24.1	-29.1	-29.1	25.7	-27.4	-33.1	-33.1	28.6
	9:12	-21.3	-25.8	-25.8	23.0	-24.1	-29.2	-29.2	25.5	-27.4	-33.1	-33.1	28.5
	10:12	-21.4	-25.8	-25.8	22.9	-24.2	-29.2	-29.2	25.4	-27.4	-33.1	-33.1	28.3
	11:12	-21.4	-25.9	-25.9	22.7	-24.2	-29.3	-29.3	25.3	-27.5	-33.2	-33.2	28.2
	12:12	-21.4	-25.9	-25.9	22.6	-24.3	-29.3	-29.3	25.2		-33.2	-33.2	28.1
H	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.
	1:12	2.0	2.0	2.0	2.0	2.1	2.2	2.6	2.8	3.0	3.5	4.0	4.6
	2:12		3.6	3.6	3.6	3.6				4.4	4.9	5.4	6.0
	3:12	5.0	5.0	5.0	5.0	5.0		5.1	5.2	5.5	6.0	6.5	7.1
	4:12	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.4	6.9	7.4	80
	5:12	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.5	8.0	8.6
	6:12	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	8.0	2.5	9.1
	7:12	7.9	7.9	7.9	7.9	7.9		7.9	7.9	7.9	8	80	9.4
	8:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	50	0.6	9.5
	9:12		8.2	8.2	8.2	8.2		8.2		8.2	200	9.0	9.6
	10:12	8.2	8.2	8.2	8.2	8.2		8.2	8.2	8.2	8.5	9.0	9.5
	11:12	8.1	8.1	8.1	8.1	8.1		8.1	8.1	8.1	8.4	6.8	9.4
	12:12	7.9	7.9	7.9	7.9	7.0							
						5:1	7.9	7.9	7.9	7.9	8.3	8.7	9.2

Lateral



East Coast (Low Snow)*

110 mph

10 psf

Basic Wind Speed

Ground Snow Load

	a n	Up Pressures (psf)	(Jsc)	Down	OD	Up Pressures (psf)	st)	Down	Up	Up Pressures (psf)	(Jst)	Down
Roof Pitch	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(bst)
1:12	-17.1	-31.8	-50.2	18.4	-17.1	-31.8	-50.2	18.4	-21.0	-38.9	-61.3	18.4
2:12	-15.2	-30.0	-46.6	17.7	-15.2	-30.0	-46.6	17.7	-18.8	-36.7	-56.8	18.6
3:12	-15.3	-30.0	-46.6	17.0	-15.3	-30.0	-46.6	17.0	-18.8	-36.7	-56.9	17.9
4:12	-15.3	-30.0	-46.6	16.2	-15.3	-30.0	-46.6	16.2	-18.8	-36.7	-56.9	17.1
5:12	-15.3	-30.1	-46.7	15.4	-15.3	-30.1	-46.7	15.4	-18.9	-36.8	-56.9	16.3
6:12	-15.4	-30.1	-46.7	14.6	-15.4	-30.1	-46.7	14.6	-18.9	-36.8	-57.0	15.5
7:12	-17.2	-20.9	-20.9	19.6	-17.2	-20.9	-20.9	19.6	-21.2	-25.7	-25.7	23.2
8:12	-17.3	-21.0	-21.0	19.5	-17.3	-21.0	-21.0	19.5	-21.2	-25.7	-25.7	23.1
9:12	-17.3	-21.0	-21.0	19.4	-17.3	-21.0	-21.0	19.4	-21.3	-25.8	-25.8	22.9
10:12	-17.4	-21.1	-21.1	19.3	-17.4	-21.1	-21.1	19.3	-21.3	-25.8	-25.8	22.8
11:12	-17.4	-21.1	-21.1	19.2	-17.4	-21.1	-21.1	19.2	-21.4	-25.8	-25.8	22.7
12:12	-17.5	-21.1	-21.1	19.1	-17.5	-21.1	-21.1	19.1	-21.4	-25.9	-25.9	22.6
1.12	2,5	0 00	64.5	10 4	24.4	45.4	20.07	10.4	20.4	22.2	010	10.4
77.7	0.12-	5.00.	C.TO-	10.4	4.47-	1.04	5.07-	10.4	4.07-	7.76-	6.10-	10.4
71.7	-18.8	-36./	-20.8	18.6	-71.9	47.5	-65./	19.9	-72.4	-49.7	-/6.0	71.4
3:12	-18.8	-36.7	-56.9	17.9	-21.9	-42.5	-65.8	19.1	-25.4	-49.2	-76.0	20.6
4:12	-18.8	-36.7	-56.9	17.1	-21.9	-45.6	-65.8	18.3	-25.5	-49.3	-76.1	19.8
5:12	-18.9	-36.8	-56.9	16.3	-22.0	-42.6	-65.8	17.6	-25.5	-49.3	-76.1	19.0
6:12	-18.9	-36.8	-57.0	15.5	-22.0	-42.6	-62.9	16.8	-25.5	-49.3	-76.1	18.3
7:12	-21.2	-25.7	-25.7	23.2	-24.6	-29.8	-29.8	26.2	-28.6	-34.5	-34.5	29.8
8:12	-21.2	-25.7	-25.7	23.1	-24.7	-29.8	-29.8	26.1	-28.6	-34.6	-34.6	29.7
9:12	-21.3	-25.8	-25.8	22.9	-24.7	-29.9	-29.9	26.0	-28.7	-34.6	-34.6	29.6
10:12	-21.3	-25.8	-25.8	22.8	-24.7	-29.9	-29.9	25.9	-28.7	-34.6	-34.6	29.5
11:12	-21.4	-25.8	-25.8	22.7	-24.8	-29.9	-29.9	25.8	-28.7	-34.7	-34.7	29.4
12:12	-21.4	-25.9	-25.9	22.6	-24.8	-30.0	-30.0	25.7	-28.8	-34.7	-34.7	29.3
	1	;		7 07	9	2				5	2	100
71:17	7.67-	4.74	-/4.0	10.4	7.67-	0.50	1.40	10.4	1.23.1	19.	2.06-	18.7
71:7	-23.1	-44./	7.60-	20.4	1.07-	-20.0	-/8.1	7.17	1.67-	57.75	-88.3	73.2
3:12	-23.1	44.8	-69.2	19.6	7.97-	-50.6	-/8.1	20.9	-29.7	-5/.3	-88.3	22.4
71:4	1.62-	0.44.0	7.60-	10.0	7.07-	0.00-	1.07-	1.02	1.67-	57.5	4.00	0.12
5:12	-23.1	44.8	-69.7	18.1	7.97-	-20.7	-/8.1	19.3	-79.8	-5/.4	-88.4	20.8
6:12	-23.2	-44.9	-69.3	17.3	-26.3	-50.7	-78.2	18.6	-29.8	-57.4	-88.4	20.4
7:12	-25.9	-31.4	-31.4	27.4	-29.4	-35.5	-35.5	30.5	-33.3	-40.2	-40.2	34.1
8:12	-26.0	-31.4	-31.4	27.3	-29.4	-35.5	-35.5	30.4	-33.3	-40.2	-40.2	34.0
9:12	-26.0	-31.4	-31.4	27.2	-29.4	-35.6	-35.6	30.3	-33.4	-40.3	-40.3	33.8
10:12	-26.1	-31.5	-31.5	27.1	-29.5	-35.6	-35.6	30.2	-33.4	-40.3	-40.3	33.7
11:12	-26.1	-31.5	-31.5	27.0	-29.5	-35.6	-35.6	30.1	-33.5	-40.4	-40.4	33.6
12:12	-26.1	-31.6	-31.6	26.9	-29.6	-35.7	-35.7	30.0	-33.5	-40.4	-40.4	33.5
Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
1:12	1.1	1.1	1.2	1.4	1.5	1.6	2.0	2.2	2.4	2.9	3.6	4.4
2:12	2.1	2.1	2.1	2.2	2.3	2.4	2.8	3.0	3.2	3.7	4.2	4.8
3:12	2.9	2.9	2.9		3.0	3.1		3.7	3.9	4.4	4.9	5.5
4:12	3.6	3.6	3.6	3.6	3.6	3.7		4.2	4.5	5.0	5.5	6.1
5:12	4.1	4.1	4.1	4.1	4.1	4.1	4.5	4.7	4.9	5.4	5.9	6.5
6:12	4.6	4.6	4.6	4.6	4.6	4.6		5.0	5.3	5.8	6.3	6.9
7:12	4.8	4.8	4.8	4.8	4.8	4.8	5.1	5.3	5.5	0.9	6.5	7.1
8:12	5.0	5.0	5.0	5.0	5.0	5.0	5.3	5.5	5.7	6.2	9.9	7.2
9:12	5.2	5.2	5.2	5.2	5.2	5.2			8.2	6.3	6.7	7.3
10:12	5.2	5.2	5.2	5.2	5.2	5.2			8.2	6.3	6.7	7.3
11:12	5.2	5.2	5.2	5.2	5.2	5.2		5.6	8.2	6.3	6.7	7.3
12:12	5.2	5.2	C		-	-						
		4:0	7:0	2.5	5.2	5.5	5.5	2.6	89.	6.2	6.7	7.2

Lateral

1.6

0.9

0.8

9.0

0.2



New Jersey (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

115 mph

25 psf

Basic Wind Speed

Ground Snow Load

		a ;	Bldg. Height = 15	= 15	ئے	<u>8</u>	Bldg. Height = 30 ft.	tht = 30		α :	Bldg. Height	9 =	٠.
	Roof Pitch	Ur Zone 1	Up Pressures (pst)	pst) Zone 3	(psd)	Up Zone 1	Up Pressures (pst)	pst) Zone 3	(pst)	Up Zone 1	Up Pressures (pst)	ost) Zone 3	(psf)
	1:12	-18.8	-34.9	-55.0	25.9	-18.8	-34.9	-55.0	25.9	-23.1	-42.7	-67.1	25.9
E	2:12	-16.8	-32.9	-51.0	24.6	-16.8	-32.9	-51.0	24.6	-20.7	-40.2	-62.2	26.2
хр	3:12	-16.8	-32.9	-51.0	23.1	-16.8	-32.9	-51.0	23.1	-20.7	-40.2	-62.3	24.7
os	4:12	-16.8	-32.9	-51.1	21.6	-16.8	-32.9	-51.1	21.6	-20.7	-40.3	-62.3	23.2
ure	5:12	-16.9	-33.0	-51.1	20.1	-16.9	-33.0	-51.1	20.1	-20.7	-40.3	-62.3	21.7
e C	6:12	-16.9	-33.0	-51.1	18.7	-16.9	-33.0	-51.1	18.7	-20.8	-40.4	-62.4	20.3
at	7:12	-19.0	-23.0	-23.0	23.5	-19.0	-23.0	-23.0	23.5	-23.3	-28.2	-28.2	26.4
eg	8:12	-19.0	-23.0	-23.0	22.3	-19.0	-23.0	-23.0	22.3	-23.3	-28.2	-28.2	25.2
ory	9:12	-19.0	-23.1	-23.1	21.3	-19.0	-23.1	-23.1	21.3	-23.4	-28.3	-28.3	24.8
<i>β</i>	10:12	-19.1	-23.1	-23.1	20.8	-19.1	-23.1	-23.1	20.8	-23.4	-28.3	-28.3	24.7
	11:12	-19.1	-23.2	-23.2	20.7	-19.1	-23.2	-23.2	20.7	-23.4	-28.3	-28.3	24.6
	12:12	-19.2	-23.2	-23.2	20.6	-19.2	-23.2	-23.2	20.6	-23.5	-28.4	-28.4	24.5
	1:12	-23.1	-42.7	-67.1	25.9	-26.8	-49.4	-77.6	25.9	-31.1	-57.2	-89.7	25.9
E	2:12	-20.7	-40.2	-62.2	26.2	-24.0	-46.6	-72.0	27.6	-27.9	-53.9	-83.2	29.2
Exp	3:12	-20.7	-40.2	-62.3	24.7	-24.0	-46.6	-72.0	26.1	-27.9	-53.9	-83.2	27.7
008	4:12	-20.7	-40.3	-62.3	23.2	-24.1	-46.6	-72.0	24.6	-28.0	-54.0	-83.2	26.2
sure	5:12	-20.7	-40.3	-62.3	21.7	-24.1	-46.7	-72.1	23.1	-28.0	-54.0	-83.3	24.7
e C	6:12	-20.8	-40.4	-62.4	20.3	-24.2	-46.7	-72.1	21.7	-28.0	-54.1	-83.3	23.3
at	7:12	-23.3	-28.2	-28.2	26.4	-27.0	-32.7	-32.7	28.9	-31.3	-37.8	-37.8	32.3
eg	8:12	-23.3	-28.2	-28.2	25.2	-27.1	-32.7	-32.7	28.3	-31.4	-37.9	-37.9	32.2
ory	9:12	-23.4	-28.3	-28.3	24.8	-27.1	-32.7	-32.7	28.2	-31.4	-37.9	-37.9	32.1
С	10:12	-23.4	-28.3	-28.3	24.7	-27.1	-32.8	-32.8	28.1	-31.5	-38.0	-38.0	32.0
	11:12	-23.4	-28.3	-28.3	24.6	-27.2	-32.8	-32.8	28.0	-31.5	-38.0	-38.0	31.8
	12:12	-23.5	-28.4	-28.4	24.5	-27.2	-32.9	-32.9	27.9	-31.5	-38.0	-38.0	31.7
	1:12	-28.3	-52.0	-81.6	25.9	-32.0	-58.7	-92.1	25.9	-36.3	-66.5	-104.2	26.9
E	2:12	-25.3	-49.0	-75.7	28.2	-28.7	-55.4	-85.4	29.6	-32.6	-62.7	-96.7	31.2
хр	3:12	-25.3	-49.1	-75.7	26.7	-28.7	-55.4	-85.5	28.1	-32.6	-62.8	-96.7	29.7
os	4:12	-25.4	-49.1	-75.8	25.1	-28.7	-55.4	-85.5	26.5	-32.6	-62.8	-96.7	28.2
ure	5:12	-25.4	-49.1	-75.8	23.7	-28.8	-55.5	-85.5	25.1	-32.7	-62.8	-96.7	26.7
e C	6:12	-25.4	-49.2	-75.8	22.3	-28.8	-55.5	-85.6	23.7	-32.7	-62.9	8.96-	25.3
ate	7:12	-28.5	-34.4	-34.4	29.9	-32.2	-38.9	-38.9	33.1	-36.5	-44.1	-44.1	36.9
ego	8:12	-28.5	-34.4	-34.4	29.6	-32.2	-38.9	-38.9	33.0	-36.6	-44.1	-44.1	36.8
ory	9:12	-28.5	-34.5	-34.5	29.5	-32.3	-39.0	-39.0	32.8	-36.6	-44.1	-44.1	36.7
D	10:12	-28.6	-34.5	-34.5	29.4	-32.3	-39.0	-39.0	32.7	-36.6	-44.2	-44.2	36.6
	11:12	-28.6	-34.6	-34.6	29.3	-32.4	-39.0	-39.0	32.6	-36.7	-44.2	-44.2	36.5
	12:12	-28.7	-34.6	-34.6	29.1	-32.4	-39.1	-39.1	32.5	-36.7	-44.3	-44.3	36.4
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12		2.0	2.0	2.0	2.1	2.2		2.8	3.0	3.5	4.0	4.6
	2:12	3.6	3.6	3.6	3.6	3.6	3.6	4.0	4.1	4.4	4.9	5.4	6.0
	3:12	2.0	2.0	2.0	2.0	2.0	2.0	5.1	5.2	5.5	0.9	6.5	7.1
Do	4:12	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.4	6.9	7.4	8.0
wr	5:12	7.0	7.0	7.0	7.0	7.0		7.0	7.0	7.0	7.5	8.0	8.6
ı S	6:12	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	8.0	8.5	9.1
lop	7:12	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	8.3	φ φ	9.4
е	8:12	8.1	8.1	8.1	8.1	8.1			8.1	8.1		9.0	9.5
	9:12		8.2		8.2	8.2				8.2		0.6	9.6
	10:12	8.2	8.2	8.2	8.2	8.2	8.2			8.2	8.5	9.0	9.5
	11:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	4.0	0.8 0.0	9.4
7	77.77	7.5		5.	51	5	\dashv	6.1	6.1	5	0:0	0.7	3.6
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	5s = 2.5	Ss = 3.1

Side Load (psf)

Lateral

0.8



Louisiana (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

120 mph

0 psf

Basic Wind Speed

Ground Snow Load

		8 d	Bldg. Height = Up Pressures (psf)	: 15	ft. Down	8 d	Bldg. Height = 30 ft.	ht = 30 f	0 '	8 d	Bldg. Height = 60		ft. Down	
	Koor Pitch	Tau07	7 au07	20ne 3	(psr)	700e 1	7 auo7	20ne 3	(psr)	700e 1	7 au07	cone 3	(pst)	
	1:12	-20.6	-38.1		13.5	-20.6	-38.1	-60.0	13.5	-25.3	-46.6		13.5	
E	2:12	-18.4	-35.9	-55.7	14.4	-18.4	-35.9	-55.7	14.4	-22.6	-43.9	62.9	16.8	
(pc	3:12	-18.4	-36.0	-55.7	14.4	-18.4	-36.0	-55./	14.4	977-	-43.9	67.9	16.7	
วรเ	4:12	-18.4	-36.0	-55./	14.3		-36.0	72.7	14.3	7.77-	-44.0	6.75	10.0	
ire	5:12	-18.5	-36.0	22.8	14.2	-18.5	-36.0	× 20.0	14.2	1.77-	-44.0	-68.0	10.5	
Ca	6:12	-18.5	-36.1	-55.8	14.1	-18.5	-36.1	55.8	14.1	1777-	-44.0	-68.0	16.4	
ate	7:12	-20.7	-25.1	-25.1	22.8	-20.7	-25.1	-25.1	22.8	-25.4	-30.8	-30.8	27.0	
go	8:12	-20.8	-25.2		22.7	-20.8	-25.2	-25.2	22.7	-25.5	-30.8	-30.8	26.9	
ry	9:12	-20.8	-25.2		27.2	-20.8	-25.2	-25.2	22.5	-25.5	-30.9	-30.9	26.8	
В	10:12	-20.9	-25.3	-25.3	22.4	-20.9	-25.3	-25.3	22.4	-25.6	-30.9	-30.9	26.7	
	11:12	-20.9	-25.3	-25.3	22.3	-20.9	-25.3	-25.3	22.3	-25.6	-30.9	-30.9	26.5	
	12:12	-21.0	-25.3	-25.3	22.2	-21.0	-25.3	-25.3	22.2	-25.7	-31.0	-31.0	26.4	
	1:12	-25.3	-46.6	-73.2	13.5	-29.3	-53.9	-84.6	13.5	-34.0	-62.4	-97.8	14.1	
	2:12	-22.6	-43.9	-67.9	16.8	-26.3	-50.8	-78.5	18.8	-30.5	-58.8	-90.7	21.2	
Ex	3:12	-22.6	-43.9	-67.9	16.7	-26.3	-50.9	-78.5	18.7	-30.5	-58.9	-90.7	21.1	
po	4.12	-227	44.0		16.6	-26.3	-509	-78.5	18.7	-306	-58.9	8 06-	21.0	
su	5.12	-227	44.0	680	16.5	-26.4	-509	-78.6	186	-30.6	-58 0	8 06-	20.0	
re	6.10	22.7	2 2	0.00	70.0	26.4	0.50	707	100	200	200	000	000	
С	5:12	1.77-	0.44.0	-68.0	10.4	-20.4	0.15-	-/8.0	18.5	-30.6	0.86-	-50.8	20.8	
ate	7:12	-25.4	-30.8	-30.8	27.0	-29.5	-35./	-35./	30.7	-34.2		-41.3	34.9	
go	8:12	-25.5	-30.8	-30.8	26.9	-29.6	-35.7	-35.7	30.5	-34.3	-41.3	-41.3	34.8	
ory	9:12	-25.5	-30.9	-30.9	26.8	-29.6	-35.7	-35.7	30.4	-34.3	-41.4	-41.4	34.7	
С	10:12	-25.6	-30.9	-30.9	26.7	-29.7	-35.8	-35.8	30.3	-34.4	-41.4	-41.4	34.6	
	11:12	-25.6	-30,9	-30.9	26.5	-29.7	-35.8	-35.8	30.2	-34.4	-41.5	-41.5	34.4	
	12:12	-25.7	-31.0	-31.0	26.4	-29.7	-35.9	-35.9	30.1	-34.4	-41.5	-41.5	34.3	
	1.12	-30 9	-56.7	0 68-	13.5	-35.0	-64.1	-100 4	14.4	-39.7	-77.5	-113.6	15.8	
	2.12	777	72.7		19.6	21.0	-F0.4	-03.1	216	35.6		-105.4	24.0	
E	21.2	1.12-	0.00	0.20	10.0	-01.4	1.00	1.00-	0.12	0.00	1.00	+.COT-	0.4.0	
(pc	3:12	1.12-	-53.5	-82.6	19.5	-31.4	-60.5	-93.2	21.6	-35.6	4.89	-105.4	23.9	
วรเ	4:12	-27.7	-53.6	-82.6	19.5	-31.4	-60.5	-93.2	21.5	-35.6	-68.5	-105.4	23.8	
ıre	5:12	-27.8	-53.6	-82.6	19.4	-31.4	-60.5	-93.2	21.4	-35.7	-68.5	-105.5	23.8	
C	6:12	-27.8	-53.6	-82.7	19.3	-31.5	9.09-	-93.3	21.3	-35.7	-68.6	-105.5	23.7	
ate	7:12	-31.1	-37.5	-37.5	32.1	-35.2	-42.4	-42.4	35.7	-39.9	-48.1	-48.1	40.0	
eg	8:12	-31.1	-37.6	-37.6	32.0	-35.2	-42.5	-42.5	35.6	-39.9	-48.1	-48.1	39.9	
ory	9:12	-31.2	-37.6	-37.6	31.8	-35.2	-42.5	-42.5	35.5	-39.9	-48.2	-48.2	39.7	
D	10:12	-31.2	-37.7	-37.7	31.7	-35.3	-42.6	-42.6	35.4	-40.0	-48.2	-48.2	39.6	
	11:12	-31.3	-37.7	-37.7	31.6	-35.3	-42.6	-42.6	35.3	-40.0	-48.2	-48.2	39.5	
	12:12	-31.3	-37.8	-37.8	31.5	-35.4	-42.6	-42.6	35.2	-40.1	-48.3	-48.3	39.4	
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1	
	1:12	0.3	0.5	0.7	6.0	1.1	1.2	1.8	2.0	2.3	2.9	3.6	4.4	
	2:12	9.0	8.0	1.0	1.2	1.4	1.5	2.1	2.3	5.6	3.3	3.9	4.7	
	3:12	0.8	1.1	1.3	1.5	1.6	1.8		2.5	2.9	3.5	4.2	5.0	
Do	4:12	1.1	1.3	1.5	1.7	1.9	2.0	5.6		3.1	3.8	4.5	5.3	
ow	5:12	1.3	1.6	1.8	2.0	2.1		2.8	3.0	3.3	4.0	4.7	5.5	
n S	6:12	1.6	1.8	2.0	2.2	2.3	2.5		3.2	3.5	4.2	4.8	5.6	
Slo	7:12	1.8	2.0	2.2	2.4	2.5	2.7	3.2	3.4	3.7	4.3	5.0	5.8	
ре	8:12	1.9	2.1	2.3	2.5	2.7	2.8	3.3	3.5	3.8	4.5	5.1	5.9	
	9:12	2.1	2.3	2.5	2.7	2.8	3.0	3.5	3.6	4.0	4.6	5.2	5.9	
	10:12	2.2		5.6	2.8	3.0	3.1	3.6	3.8	4.1	4.7	5.3	6.0	
	11:12	2.4	2.6	2.7	2.9	3.1	3.2	3.7	3.8	4.1	4.7	5.3	6.0	
	12:12	2.5	2.7	2.8	3.0	3.2	3.3	3.7	3.9	4.2	4.8	5.4	6.1	
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1	
		0	(0	0	0	,	,	0	0	0	•	

Up and Down (psf)

Side Load (psf)

Lateral

2.6

0.9

0.8

9.0

0.4

0.2



7.05 ASCE

Florida (Typical)*
APPENDIX - Pressure Tables for Flush Nounted Roof Systems

140 mph

0 psf

Basic Wind Speed

Ground Snow Load

Down Up Pressures psf Down Down Zone	= 15 ft.		Bldg. Height = 30 ft.	ht = 30 1		8	Bldg. Height = 60	= 60	نے
1:12	cone 3	-		osf) Zone 3	(pst)	Up Zone 1	Up Pressures (psf)	osf) Zone 3	(psf)
2.12 -25.5 49.4 -76.3 18.4 -25.5 49.4 -76.3 18.4 -25.5 49.4 -76.3 18.3 -25.5 49.4 -76.3 18.3 -25.5 49.4 -76.3 18.3 -25.5 49.5 -76.4 18.1 -25.6 49.5 -76.4 18.1 -25.6 49.5 -76.4 18.1 -25.6 49.5 -76.4 18.1 -25.6 49.5 -76.4 18.1 -25.6 49.5 -76.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 18.1 -25.6 49.5 -26.4 -27.7 -27.7 -27.7 -27.8 -28.9 -20.9 -20.7 -27.8 -27.9 -27.7	-82	Ë	Н	-82.2	13.5	-34.9	-63.9	-100.1	14.4
3:12 -25.5 49.4 -76.3 18.3 -25.5 4:12 -25.6 49.4 -76.3 18.2 -25.6 4:12 -25.6 49.5 -76.4 18.2 -25.6 5:12 -25.6 49.5 -76.4 18.1 -25.6 6:12 -25.6 49.5 -76.4 18.1 -25.6 7:12 -28.7 -34.6 -34.6 29.9 -28.7 3:12 -28.7 -34.7 -34.7 -29.9 -28.7 3:12 -28.8 -34.8 -34.9 -29.9 -28.7 10:12 -28.8 -34.8 -34.9 -29.9 -28.9 11:12 -28.9 -34.9 -34.9 -29.9 -28.9 11:12 -38.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9 -34.9	-76.3		LC.	-76.3	18.4	-31.3	-60.3	-92.9	21.6
4:12 -25.6 -49.4 -76.3 18.2 -25.6 -49.5 -76.4 18.2 -25.6 -6.12 -25.6 -49.5 -76.4 18.1 -25.6 -6.12 -25.6 -49.5 -76.4 18.1 -25.6 -6.12 -25.6 -49.5 -76.4 18.1 -25.6 -6.6 -25.7 -28.7 -28.7 -28.8 -29.9 -28.7 -28.8 -28.8 -29.9 -28.9<	-76.			-76.3	18.3	-31.3	-60.3	-92.9	21.5
5:12 -25.6 -49.5 -76.4 18.2 -25.6 -49.5 -76.4 18.1 -25.6 -49.5 -76.4 18.1 -25.6 -49.5 -76.4 18.1 -25.6 -49.5 -76.4 18.1 -25.6 -49.5 -77.2 -88.1 -34.7 -34.7 -29.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.7 -28.8 -28.9 -28.9 -28.9 -28.9 -28.9 -28.9 -28.9 -28.8 -28.9	-76.		-49	-76.3	18.2	-31.3	-60.3	-93.0	21.4
6:12	-	-	·	-76.4	18.2	-31.4	-60.4	-93.0	21.4
7:12 -28.7 -34.6 -39.6 -28.7 -28.7 8:12 -28.8 -34.7 -34.7 -28.8 -28.8 9:12 -28.8 -34.9 -34.7 -29.7 -28.8 10:12 -28.8 -34.8 -34.8 -29.6 -28.8 11:12 -28.9 -34.9 -29.3 -28.9 -28.8 11:12 -28.9 -34.9 -29.9 -21.6 -38.9 11:12 -34.9 -63.9 -100.1 14.4 -40.4 -28.3 11:12 -34.9 -63.9 -100.1 14.4 -40.4 -28.3 11:12 -31.3 -60.3 -92.9 21.6 -36.3 -36.3 2:12 -31.3 -60.3 -92.9 21.6 -38.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3 -36.3	-76.4	-	-	-76.4	18.1	-31.4	-60.4	-93.0	21.3
8:12 - 28.7 -34.7 -34.7 29.8 -28.7 -28.8 -28.8 -28.8 -34.8 -34.8 -34.8 -29.6 -28.8 -29.1 10.12 -28.8 -34.8 -34.8 -34.8 -29.6 -28.8 -29.1 11.12 -28.8 -34.9 -34.9 -34.9 29.3 -28.9 -29.1 11.12 -28.9 -34.9 -34.9 29.3 -28.9 -29.9 21.2 -21.3 -60.3 -29.9 21.5 -36.3 -21.2 -21.3 -60.3 -29.9 21.5 -36.3 -21.2 -21.3 -60.3 -29.9 21.5 -36.3 -21.2 -21.3 -60.3 -29.9 21.5 -36.3 -21.2 -21.3 -60.3 -29.9 21.5 -36.3 -21.2 -21.3 -60.4 -29.0 21.4 -36.3 -21.2 -21.3 -60.4 -29.0 21.4 -36.3 -21.2 -21.3 -40.4 -22.4	-		_	-34.6	29.9	-35.1	-42.3	-42.3	35.6
10.12 -28.8 -34.7 -34.7 -34.8 -28.8 -34.			Ľ	-34.7	29.8	-35.1	-42.4	-42.4	35.5
1011 - 28.8 - 34.8	-34.7			-34.7	29.7	-35.2	-42.4	-42.4	35.4
11:12 -28.8 -34.8 -34.8 29.4 -28.8 -28.1 -28.9 -34.9 -34.9 29.3 -28.9 -28.9 -28.9 -29.9 -29.9				-34.8	29.6	-35.2	-42.4	-42.4	35.3
12.12 -28.9 -34.9 -24.9 29.3 -28.9 -28.9 12.12 -34.9 -63.9 -100.1 14.4 -40.4 -2.12 2.112 -31.3 -60.3 -92.9 21.6 -36.3 -36.3 -31.3 -60.3 -92.9 21.5 -36.3 -36.3 -36.3 -32.9 -21.5 -36.3 -36.3 -32.9 -21.5 -36.3 -32.9 -21.5 -36.3 -22.12 -32.3 -32.3 -22.3	'	_	_	-34.8	29.4	-35.2	-42.5	-42.5	35.2
1:12	-34.9	_	_	-34.9	29.3	-35.3	-42.5	-42.5	35.1
2:12 31.3 60.3 92.9 21.6 36.3 + 4.12 31.3 60.3 92.9 21.5 36.3 + 4.12 31.3 60.3 92.9 21.5 36.3 + 4.12 31.3 60.3 92.9 21.5 36.3 + 4.12 31.3 60.3 92.0 21.4 36.3 + 4.12 31.4 60.4 -93.0 21.3 3.6.40.6 -93.0 21.3 3.6.40.6 -93.1 3.5.1 42.4 42.4 35.3 40.7 -91.2 35.1 42.4 42.4 35.3 40.7 -91.2 35.2 42.4 42.4 35.3 40.7 -4.12 35.2 42.5 42.5 35.2 40.8 -11.12 35.2 42.5 42.5 35.1 40.8 -11.12 35.2 42.5 35.1 40.8 -11.12 38.2 -73.3 -112.9 25.4 43.2 43.2 42.1 38.2 -73.3 -112.9 25.4 43.2 43.2 42.1 38.2 -73.3 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.2 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 43.3 -12.1 38.3 -73.4 -112.9 25.3 35.8 0.4 48.5 -12.1 38.3	-	Н	Н	-115.7	16.0	-46.8	-85.4	-133.6	17.9
3:12 -31.3 -60.3 -92.9 21.5 -36.3 -4.12 -31.3 -60.4 -93.0 21.4 -36.3 -4.2 -31.4 -60.4 -93.0 21.4 -36.3 -4.2 -31.3 -60.4 -93.0 21.4 -36.3 -4.2 -31.3 -60.4 -93.0 21.3 -36.4 -36.3 -4.2 -35.1 -4.2 -35.1 -4.2 -35.1 -4.2 -35.1 -4.2 -35.1 -4.2 -35.1 -4.2 -35.2 -4.2 -4.2 -3.5 -40.0 -3.1 -35.1 -35.2 -4.2 -4.2 -4.2 -3.5 -40.0 -3.1 -35.2 -4.2 -4.2 -4.2 -4.2 -4.2 -4.2 -4.2 -4				-107.3	24.3	-42.0	-80.6	-123.9	27.5
4:12 - 31.3 - 60.3 - 93.0	Н	H	Н	-107.3	24.3	-42.0	-80.6	-124.0	27.5
5:12 -314 -604 -93.0 21.4 -36.3 -4 6:12 -314 -604 -93.0 21.4 -36.3 -4 6:12 -314 -604 -93.0 21.3 -36.4 -4 7:12 -35.1 -42.3 -42.4 35.5 -40.6 -4 8:12 -35.2 -42.4 35.3 -40.7 -4			-	-107.4	24.2	-42.1	-80.6	-124.0	27.4
6:12 -31.4 -60.4 -93.0 21.3 -36.4 -7.12 -35.1 -42.3 -42.3 35.6 -40.6 -40.6 -9.12 -35.1 -42.4 -42.4 35.5 -40.7 -9.12 -35.2 -42.4 -42.4 35.5 -40.7 -9.12 -35.2 -42.4 -42.4 35.5 -40.7 -10.12 -35.2 -42.4 -42.4 35.5 -40.7 -10.12 -35.2 -42.4 -42.4 35.3 -40.7 -11.12 -35.2 -42.5 -42.5 35.1 -40.8 -11.12 -35.2 -42.5 35.1 -40.8 -11.12 -35.3 -42.5 -42.5 35.1 -40.8 -11.12 -35.3 -42.5 -42.5 35.1 -40.8 -11.12 -35.3 -42.5 -42.5 35.1 -40.8 -11.12 -38.2 -73.3 -112.9 25.4 -43.2 -43.2 -12.9 25.4 -43.2 -43.2 -12.9 25.4 -43.2 -43.2 -12.9 25.4 -43.2 -42.5 33.1 -12.9 25.4 -43.2 -42.5 -12.9 25.1 -43.3 -12.9 25.4 -43.2 -42.8 -51.5 -51.5 -51.7 -42.9 -51.7 -51.7 -42.0 -48.3 -12.9 25.1 -42.8 -51.6 -51.6 -51.6 -42.3 -42.8 -42.9 -51.7 -51.7 -42.0 -48.5 -42.9 -51.7 -51.7 -42.0 -48.5 -42.9 -51.7 -51.7 -42.0 -48.5 -42.9 -51.7 -51.7 -42.0 -42.5 -51.7 -42.0 -51.7 -51.7 -42.0 -42.5 -51.7 -42.0 -42.5 -42.8 -42.0 -42.5 -	H.	H.	-	-107.4	24.1	-42.1	-80.7	-124.0	27.3
7:12 -35.1	-93.0			-107.4	24.0	-42.1	-80.7	-124.1	27.2
8:12 -35.1	-42.3	·		-49.0	40.6	-47.0	-56.6	-56.6	46.4
9:12 -35.2	-45.	Ė	_	-49.0	40.5	-47.0	-56.7	-56.7	46.3
10:12	-42.4	Ė	Ė	-49.1	40.4	-47.1	-56.7	-56.7	46.2
11:12 -35.2 -42.5 -42.5 35.2 -40.8 -11:12 -35.3 -42.5 -42.5 35.1 -40.8 -11:12 -35.3 -42.5 -42.5 35.1 -40.8 -11:12 -38.2 -77.7 -121.6 16.7 -48.1 -12:12 -38.2 -73.3 -112.9 25.4 -43.2 -12:12 -38.2 -73.3 -112.9 25.4 -43.2 -13:12 -38.2 -73.4 -112.9 25.4 -43.2 -13:12 -38.3 -73.4 -112.9 25.2 -43.3 -13:12 -38.3 -73.4 -112.9 25.2 -43.3 -43.2 -13:12 -42.8 -51.6 -51.6 -51.6 -42.4 -48.3 -13:12 -42.8 -51.6 -51.6 -51.6 -42.4 -48.3 -11:12 -42.8 -51.6 -51.7 -51.7 -42.1 -48.3 -11:12 -42.9 -51.7 -51.7 -42.1 -48.5 -11:12 -42.9 -51.7 -51.7 -42.1 -48.5 -11:12 -42.9 -51.7 -51.7 -42.1 -48.5 -11:12 -42.9 -51.7 -51.7 -51.7 -42.1 -48.5 -11:12 -42.9 -51.7 -51.7 -51.7 -42.1 -48.5 -11:12 -42.9 -51.7 -51.7 -51.7 -42.9 -11.1 -51.7 -51.	4 -42.4			-49.1	40.3	-47.1	-56.8	-56.8	46.1
12:12	5 -42.5		_	-49.1	40.2	-47.2	-56.8	-56.8	46.0
1:12	-45.	÷	_	-49.2	40.1	-47.2	-56.9	-56.9	45.8
2:12 -38.2 -73.3 -112.9 25.4 43.2 -43.12 -38.2 -73.3 -112.9 25.4 43.2 -43.12 -38.2 -73.4 -112.9 25.3 43.2 -43.2 -43.2 -43.3 -112.9 25.2 43.3 -43.2 -42.2 -38.3 -73.4 -112.9 25.2 43.3 -43.2 -42.2 -38.3 -73.4 -113.0 25.1 43.3 -42.2 -42.8 -51.6 -51.6 42.4 48.3 -9.12 -42.8 -51.6 -51.6 42.3 48.4 -111.12 -42.9 -51.7 -51.7 42.2 48.4 -111.12 -42.9 -51.7 -51.7 42.2 48.4 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 48.5 -111.12 -42.9 -51.7 -51.7 42.0 -48.5 -111.12 -42.9 -51.7 -51.7 42.0 -48.5 -111.12 -42.9 -51.7 -51.7 -42.0 -42.9 -51.7 -51.7 -42.0	-121.6	H	Ë	-137.2	18.3	-54.5	-99.2	-155.1	20.2
3:12 -38.2 -73.3 -112.9 25.4 43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.2 -43.3 -43.2 -43.3 -43.2 -43.3 -43.2 -43.3 -43.3 -43.2 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.4 -48.3 -48.4 -48.4 -48.3 -48.4 -48.4 -48.4 -48.3 -48.4 -	Н	Ė	Ė	-127.3	28.2	-48.9	-93.6	-143.9	31.4
4:12 -38.2 -73.4 -112.9 25.3 43.2 -73.4 -112.9 25.2 43.3 -42.7 -51.5 -112.9 25.2 43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -43.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48.3 -48.4 -48	-112.9		·	-127.3	28.1	-48.9	-93.6	-143.9	31.3
6:12 -38.3 -73.4 -112.9 25.2 43.3 -4 6:12 -38.3 -73.4 -112.0 25.1 43.3 -4 7:12 -42.7 -51.5 -51.6 -48.3 -3 -4 8:12 -42.8 -51.6 -51.6 42.4 48.3 9:12 -42.8 -51.6 -51.6 42.4 48.3 10:12 -42.8 -51.6 -51.7 42.3 48.4 10:12 -42.9 -51.7 -51.7 42.3 48.4 11:12 -42.9 -51.7 -51.7 42.0 48.5 11:12 -42.9 -51.7 -51.7 42.0 48.5 11:12 -42.9 -51.7 -51.7 42.0 48.5 11:12 -0.6 0.8 1.0 1.2 1.4 2:12 0.8 1.1 1.3 1.5 1.6	-112.9	_	_	-127.3	28.1	-49.0	-93.7	-144.0	31.3
6:12 -38.3 -73.4 -113.0 25.1 43.3 -73.4 -113.0 25.1 43.3 -73.1 -73.2 -42.5 -51.5 -51.5 42.6 48.3 -73.4 -12.8 -51.6 -51.6 42.4 -48.3 -73.4 -10.12 -42.8 -51.6 -51.6 42.3 -48.4 -710.12 -42.9 -51.7 -51.7 42.2 48.4 -711.12 -42.9 -51.7 -51.7 42.2 48.4 -712.12 -43.0 -51.7 -51.7 42.0 48.5 -71.1 12.12 0.3 0.5 0.7 0.9 1.1 -71.2 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 1.2 1.4 3.12 0.8 1.0 2.2 2.4 2.5 3.0 3.1 1.11 2.2 2.4 2.6 2.8 3.0 3.1 1.11 2.2 2.4 2.6 2.8 3.0 3.2 1.11 2.4 2.6 2.7 2.8 3.0 3.2 1.11 2.2 2.5 2.7 2.8 3.0 3.2 1.11 2.2 2.5 2.7 2.8 3.0 3.2 1.11 2.2 2.5 2.7 2.8 3.0 3.2 1.11 2.2 2.5 2.7 2.8 3.0 3.2 1.11 2.2 2.5 2.7 2.8 3.0 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2		-	m	-127.4	28.0	-49.0	-93.7	-144.0	31.2
7:12 42.7 -51.5 -51.5 42.6 48.3 -8.3 8:12 -42.8 -51.6 -51.6 42.4 48.3 -8.3 9:12 -42.8 -51.6 -51.6 42.3 48.4 -9.1 10:12 -42.9 -51.7 -51.7 42.2 48.4 -9.4 11:12 -42.9 -51.7 -51.7 42.2 48.4 -9.4 11:12 -42.9 -51.7 -51.7 42.2 48.4 -9.4 11:12 -42.9 -51.7 -51.7 42.0 48.5 -9.4 11:12 -43.0 -51.7 -51.7 42.0 48.5 -9.4 11:12 0.3 0.5 0.7 0.9 1.1 1.4 2:12 0.6 0.8 1.0 1.2 1.4 3:12 0.8 1.1 1.3 1.5 1.6 4:12 1.1 1.3 1.5 1.7 1.9 5:12<		-	m	-127.4	27.9	-49.1	-93.8	-144.0	31.1
8:12	-51.5	\dashv		-58.2	47.5	-54.7	-65.9	-65.9	53.3
9:12	-51.6		-	-58.2	47.4	-54.7	-65.9	-65.9	53.2
10:12	-	-	-58	-58.3	47.3	-54.8	-65.9	-65.9	53.1
11:12	-51.7	-	-	-58.3	47.2	-54.8	-66.0	-66.0	53.0
12:12	-51.7	÷	-	-58.4	47.1	-54.9	-66.0	-66.0	52.9
Roof Pitch Ss = 0.0 Ss = 0.1 Ss = 0.3 Ss = 0.4 Ss = 0.4 II.12 0.6 0.8 1.0 1.2 1.4 II.2 0.6 0.8 1.0 1.2 1.4 II.3 1.5 1.6 II.4 II.3 1.5 1.6 II.6 II.8 2.0 2.2 2.3 Ss = 1.3 II.8 2.0 2.1 II.8 2.0 2.2 2.3 Ss = 1.4 II.8 2.0 2.2 2.3 II.8 2.0 2.2 2.3 Ss = 1.5 II.8 2.0 2.1 II.8 2.0 2.2 2.4 2.5 2.7 2.8 II.12 2.4 2.6 2.8 3.0 III.12 2.4 2.6 2.7 2.9 3.1 II.12 2.4 2.6 2.7 2.9 3.1 II.12 2.5 2.7 2.8 3.0 3.2 II.12 2.5 2.7 2.8 3.0 3.2	-51.7	_	5 -58	-58.4	47.0	-54.9	-66.1	-66.1	52.8
1:12 0.3 0.5 0.7 0.9 1.1 2:12 0.6 0.8 1.0 1.2 1.4 3:12 0.8 1.1 1.3 1.5 1.6 4:12 1.1 1.3 1.5 1.6 1.6 5:12 1.3 1.6 1.8 2.0 2.1 1.9 6:12 1.6 1.8 2.0 2.2 2.3 1.7 1.9 7:12 1.8 2.0 2.2 2.4 2.5 2.7 2.8 8:12 1.9 2.1 2.3 2.5 2.7 2.8 3.0 9:12 2.1 2.3 2.5 2.7 2.8 3.0 1.1 10:12 2.4 2.6 2.7 2.9 3.1 1.2 2.5 2.7 2.8 3.0 3.2 12:12 2.5 2.7 2.8 3.0 3.2 2.1 2.2 2.2 2.3 3.2 2.2	Ss = 0.2	SS	Ss = 0.	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
2:12 0.6 0.8 1.0 1.2 1.4 3:12 0.8 1.1 1.3 1.5 1.6 1.6 4:12 1.1 1.3 1.5 1.7 1.9 5:12 1.3 1.6 1.8 2.0 2.1 6:12 1.6 1.8 2.0 2.1 2.3 7:12 1.8 2.0 2.2 2.3 8:12 1.9 2.1 2.3 2.5 2.7 8:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0	2	6	1	1.8	2.0	2.3	2.9	3.6	4.4
3:12 0.8 1.1 1.3 1.5 1.6 4:12 1.1 1.3 1.5 1.7 1.9 5:12 1.3 1.6 1.8 2.0 2.1 6:12 1.6 1.8 2.0 2.2 2.3 7:12 1.8 2.0 2.2 2.3 8:12 1.9 2.1 2.3 2.5 2.7 9:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0 3.2		_	-1	2.1	2.3	5.6	3.3	3.9	4.7
4:12 1.1 1.3 1.5 1.7 1.9 5:12 1.3 1.6 1.8 2.0 2.1 6:12 1.6 1.8 2.0 2.2 2.3 7:12 1.8 2.0 2.2 2.3 8:12 1.9 2.1 2.3 2.5 2.7 9:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0 3.2				2.3	2.5	2.9	3.5	4.2	2.0
5:12 1.3 1.6 1.8 2.0 2.1 6:12 1.6 1.8 2.0 2.2 2.3 7:12 1.8 2.0 2.2 2.4 2.5 8:12 1.9 2.1 2.3 2.5 2.7 9:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0 3.2			_	2.6	2.8	3.1	3.8	4.5	5.3
6:12 1.6 1.8 2.0 2.2 2.3 7:12 1.8 2.0 2.2 2.4 2.5 8:12 1.9 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.7 2.8 3.0 11:12 2.4 2.6 2.7 2.8 3.0 12:12 2.5 2.7 2.8 3.0 3.2 12:12 2.5 2.7 2.8 3.0 3.2			2.	2.8	3.0	3.3	4.0	4.7	5.5
7:12 1.8 2.0 2.2 2.4 2.5 8:12 1.9 2.1 2.3 2.5 2.7 9:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0 3.2				3.0	3.2	3.5	4.2	4.8	5.6
8:12 1.9 2.1 2.3 2.5 2.7 2.8 10:12 2.1 2.3 2.5 2.7 2.8 10:12 2.2 2.4 2.6 2.8 3.0 11:12 2.4 2.6 2.7 2.9 3.1 12:12 2.5 2.7 2.8 3.0 3.2				3.2	3.4	3.7	4.3	2.0	5.8
2.1 2.3 2.5 2.7 2.8 2.0 2.4 2.6 2.8 3.0 2.4 2.6 2.7 2.9 3.1 2.5 2.7 2.8 3.0 3.2 2.5 2.7 2.8 3.0 3.2 2.5 2.7 2.8 3.0 3.2 2.5 2.7 2.8 3.0 3.2 2.5 2.7 2.8 3.0 3.2 3.2 3.0 3.2 3.2 3.0 3.2 3.2 3.2 3.0 3.2 3.2 3.0 3.2 3.2 3.0 3.2 3.2 3.0 3.2 3.2 3.0 3.2 3.2 3.2 3.0 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2				3.3	3.5	3.8	4.5	5.1	5.9
2.2 2.4 2.6 2.8 3.0 2.4 2.6 2.7 2.9 3.1 2.5 2.7 2.8 3.0 3.2	-	\dashv	-	3.5	3.6	4.0	4.6	5.2	5.9
2.4 2.6 2.7 2.9 3.1 2.5 2.7 2.8 3.0 3.2				3.6	3.8	4.1	4.7	5.3	6.0
2.5 2.7 2.8 3.0 3.2	+	+	w,	3.7	3.8	4.1	4.7	5.3	0.9
0 00 0 00 0			3.	3.7	3.9	4.2	4.8	5.4	6.1
Ss = 0.3 Ss = 0.4 Ss	Ss = 0.2	S	3.4 Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1

Up and Down (psf)

Side Load (psf)

Lateral

2.0

1.6

0.9

0.8

9.0



7-10 ASCE

California (Typical)*

110 mph

5 psf

Basic Wind Speed

Ground Snow Load

Down (nef)	14.8	14.4	14.0	13.5	13.2	13.0	15.4	15.3	15.2	15.0	14.9	14.8	14.8	14.4	14.0	13.5	13.2	13.0	19.4	19.3	19.1	19.0	18.9	18.8	14.8	15.0	14.5	14.1	13.9	13.8	21.9	21.8	21.7	21.6	21.5	21.3	Ss = 3.1	4.8	5.2	5.5	5.8	6.0	6.2	6.3	6.5	6.5	9.9	9.9	6. / Sc = 3.1
= 60 ft.	-36.3		-33.7	-33.7	-33.7	-33.8	-15.0	-15.0	-15.1	-15.1	-15.2	-15.2	-48.7	-45.1	-45.2	-45.2	-45.2	-45.3	-20.3	-20.4	-20.4	-20.4	-20.5	-20.5	-56.7	-52.5	-52.6	-52.6	-52.6	-52.7	-23.7	-23.8	-23.8	-23.8	-23.9	-23.9	Ss = 2.5 S	4.0	4.3	4.6	4.9	5.2	5.4	9.6	5.7	5.8	5.8	6.9	5.5 S
Bldg. Height = 60	-22.9	-21.6	-21.6	-21.6	-21.6	-21.7	-15.0	-15.0	-15.1	-15.1	-15.2	-15.2	-30.9	-29.1	-29.1	-29.1	-29.2	-29.2	-20.3	-20.4	-20.4	-20.4	-20.5	-20.5	-36.0	-33.9	-33.9	-34.0	-34.0	-34.0	-23.7	-23.8		-23.8	-23.9	-23.9	Ss = 2.0	3.2	3.6	3.9	4.3	4.6	4.9	5.1	5.2	5.3		5.3	0
Bl Upp	-12.1	-10.8	-10.8	-10.9	-10.9	-10.9	-12.3	-12.4	-12.4	-12.4	-12.5	-12.5	-16.6	-14.8	-14.8	-14.8	-14.9	-14.9	-16.7	-16.8	-16.8	-16.9	-16.9	-16.9	-19.4	-17.4	-17.4	-17.4	-17.4	-17.5	-19.6	-19.6	-19.7	-19.7	-19.7	-19.8	Ss = 1.5	2.5	5.9	3.4	3,8	4.1	4.3	4.5	4.7	4.8	4.8	6.4	Sc= 1.5
t. Down (osf)	14.8	14.4	14.0	13.5	13.2	13.0	13.3	13.2	13.0	12.9	12.8	12.7	14.8	14.4	14.0	13.5	13.2	13.0	17.3	17.1	17.0	16.9	16.8	16.7	14.8	14.4	14.0	13.5	13.2	13.0	19.8	19.7	19.6	19.4	19.3	19.2	Ss = 1.25	2.1	5.6	3.1	3.5	3.8	4.1	4.3	4.4	4.5	4.6	9.4	4.b
nt = 30 f	-29.7	-27.5			-27.6	-27.6	-12.2	-12.2	-12.2	-12.3	-12.3	-12.4	-42.1	-39.0	-39.0	-39.0	-39.1	-39.1	-17.5	-17.5	-17.6	-17.6	-17.6	-17.7	-50.0	-46.4	-46.4	-46.4	-46.5	-46.5	-20.9	-20.9	-21.0	-21.0	-21.0	-21.1	Ss = 1.0	1.9	2.4	5.9	3.3	3.7	3.9	4.1	4.3	4.4			4.5 Sc = 1.0
Bldg. Height = 30	-18.6	-17.5	-17.6	-17.6	-17.6	-17.7	-12.2	-12.2	-12.2	-12.3	-12.3	-12.4	-26.6	-25.1	-25.1	-25.1	-25.1	-25.2	-17.5	-17.5	-17.6	-17.6	-17.6	-17.7	-31.7	-29.9	-29.9	-29.9	-30.0	-30.0	-20.9	-20.9	-21.0	-21.0	-21.0	-21.1	Ss = 0.5	1.4	2.0	2.5	5.9	3.2	3.5	3.7	3.8	3.9	4.0	4.1	4.1 Sc = 0.5
Blc Up F	8.6-	-8.7	-8.7	-8.7	8.8	8.8	6.6-	-10.0	-10.0	-10.1	-10.1	-10.2	-14.2	-12.7	-12.7	-12.7	-12.7	-12.8	-14.4	-14.4	-14.5	-14.5	-14.5	-14.6	-17.0	-15.2	-15.2	-15.3	-15.3	-15.3	-17.2	-17.3		-17.3	-17.4	-17.4	Ss = 0.4	1.3	1.9	2.4	2.8	3.1	3.4	3.6	3.7	3.8	3.9	0.4	4.0 Sc = 0.4
Down (nsf)	14.8	14.4	14.0	13.5	13.2	13.0	13.3	13.2	13.0	12.9	12.8	12.7	14.8	14.4	14.0	13.5	13.2	13.0	15.4	15.3	15.2	15.0	14.9	14.8	14.8	14.4	14.0	13.5	13.2	13.0	18.0	17.8	17.7	17.6	17.5	17.4	Ss = 0.3	1.1	1.7	2.2	5.6	3.0	3.2	3.4	3.6	3.7	3.8	ω. ω.	3.9 Sc = 0.3
nt = 15 fi	- 29.7	-27.5	-27.5		-27.6	-27.6	-12.2	-12.2	-12.2	-12.3	-12.3	-12.4	-36.3	-33.6	-33.7	-33.7	-33.7	-33.8	-15.0	-15.0	-15.1	-15.1	-15.2	-15.2	-44.3	-41.0	-41.1	-41.1	-41.1	-41.2	-18.4	-18.5	-18.5	-18.5	-18.6	-18.6	Ss = 0.2	1.0	1.6	2.0	2.5	2.8	3.1	3.3	3.4	3.6	3.6	3.7	3.7 Sc=0.7
Bldg. Height = 15	-18.6	-17.5	-17.6	-17.6	-17.6	-17.7	-12.2	-12.2	-12.2	-12.3	-12.3	-12.4	-22.9	-21.6	-21.6	-21.6	-21.6	-21.7	-15.0	-15.0	-15.1	-15.1	-15.2	-15.2	-28.0	-26.4	-26.4	-26.4	-26.5	-26.5	-18.4	-18.5	-18.5	-18.5	-18.6	-18.6	Ss = 0.1	8.0	1.4	1.9	2.4	2.8	3.1	3.3	3.4	3.5	3.6	3.7	3.7 Sc = 0.1
Blo Up F	8.6-	-8.7	-8.7	-8.7	-8.8	-8.8	6.6-	-10.0	-10.0	-10.1	-10.1	-10.2	-12.1	-10.8	-10.8	-10.9	-10.9	-10.9	-12.3	-12.4	-12.4	-12.4	-12.5	-12.5	-15.0	-13.4	-13.4	-13.4	-13.5	-13.5	-15.2	-15.2	-15.2	-15.3	-15.3	-15.4	Ss = 0.0	0.7	1.4	1.9	2.4	2.8	3.1	3.3	3.4	3.5		3.7	3.7 Se = 0.0
Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12
			Exp	oos	sure	e C	Cat	eg	ory	/ B				E	xp	os	ure	e C	ate	ege	ory	C			_	E	Exp	oos	sure	e C	ate	ego	ory	D							Do)WI	n S	lop	oe				

Up and Down (psf)

Side Load (psf)

Lateral

6.0

0.7

0.5

0.2



Southwest (Typical)*

115 mph

5 psf

Basic Wind Speed

Ground Snow Load

		8 5	Bldg. Height	= 15	ft. Down	8	Bldg. Height = 30 ft.	ht = 30 f	it. Down	8 5	Bldg. Height = 60	09 =	ft. Down
	Roof Pitch	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)
	1:12	-10.8	-20.5	-32.6	14.8	-10.8	-20.5	-32.6	14.8	-13.4	-25.1	-39.8	14.8
E	2:12	9.6-	-19.3	-30.2	14.4	9.6-	-19.3	-30.2	14.4	-11.9	-23.7	-36.9	14.4
хр	3:12	9.6-	-19.3	-30.2	14.0	9.6-	-19.3	-30.2	14.0	-12.0	-23.7	-36.9	14.0
os	4:12	-9.7	-19.3	-30.2	13.5	-9.7	-19.3	-30.2	13.5	-12.0	-23.7	-36.9	13.5
ur	5:12	-9.7	-19.4	-30.2	13.2	-9.7	-19.4	-30.2	13.2	-12.0	-23.8	-37.0	13.2
e C	6:12	-9.7	-19.4	-30.3	13.0	-9.7	-19.4	-30.3	13.0	-12.1	-23.8	-37.0	13.0
at	7:12	-11.0	-13.4	-13.4	14.2	-11.0	-13.4	-13.4	14.2	-13.6	-16.5	-16.5	16.5
eg	8:12	-11.0	-13.4	-13.4	14.1	-11.0	-13.4	-13.4	14.1	-13.6	-16.5	-16.5	16.4
ory	9:12	-11.1	-13.5	-13.5	14.0	-11.1	-13.5	-13.5	14.0	-13.6	-16.6	-16.6	16.3
<i>у</i> В	10:12	-11.1	-13.5	-13.5	13.8	-11.1	-13.5	-13.5	13.8	-13.7	-16.6	-16.6	16.2
	11:12	-11.1	-13.6	-13.6	13.7	-11.1	-13.6	-13.6	13.7	-13.7	-16.7	-16.7	16.0
	12:12	-11.2	-13.6	-13.6	13.6	-11.2	-13.6	-13.6	13.6	-13.8	-16.7	-16.7	15.9
	4.40	10,	25.4	0 00	0 44	9 24	000	101	140	100	33.0	V 02	9 7 9
	71:1	-13.4	1.62-	-39.8	14.8	-T2.6	7.67-	1.04-	14.8	-18.2		-53.4	14.0
E	2:12	-11.9	-23.7	-36.9	14.4	-14.0	-27.5	-42.7	14.4	-16.3	-31.9	-49.5	14.5
хр	3:12	-12.0	-23.7	-36.9	14.0	-14.0	-27.5	-42.7	14.0	-16.3	-31.9	-49.5	14.1
os	4:12	-12.0	-23.7	-36.9	13.5	-14.0	-27.5	-42.8	13.5	-16.3	-32.0	-49.5	13.6
ure	5:12	-12.0	-23.8	-37.0	13.2	-14.0	-27.6	-42.8	13.2	-16.4	-32.0	-49.5	13.3
e C	6:12	-12.1	-23.8	-37.0	13.0	-14.1	-27.6	-42.8	13.0	-16.4	-32.0	-49.6	13.2
at	7:12	-13.6	-16.5	-16.5	16.5	-15.8	-19.2	-19.2	18.6	-18.4	-22.3	-22.3	20.9
eg	8:12	-13.6	-16.5	-16.5	16.4	-15.9	-19.2	-19.2	18.4	-18.4	-22.3	-22.3	20.8
ory	9:12	-13.6	-16.6	-16.6	16.3	-15.9	-19.3	-19.3	18.3	-18.5	-22.4	-22.4	20.6
C	10:12	-13.7	-16.6	-16.6	16.2	-15.9	-19.3	-19.3	18.2	-18.5	-22.4	-22.4	20.5
	11:12	-13.7	-16.7	-16.7	16.0	-16.0	-19.4	-19.4	18.1	-18.6	-22.5	-22.5	20.4
1	12:12	-13.8	-16.7	-16.7	15.9	-16.0	-19.4	-19.4	17.9	-18.6	-22.5	-22.5	20.3
	1:12	-16.5	-30.7	-48.5	14.8	-18.7	-34.8	-54.8	14.8	-21.3	-39.4	-62.1	14.8
E	2:12	-14.7	-29.0	-45.0	14.4	-16.8	-32.8	-50.8	14.7	-19.1	-37.2	-57.5	15.7
ΣXΕ	3:12	-14.8	-29.0	-45.0	14.0	-16.8	-32.8	-50.8	14.3	-19.1	-37.2	-57.6	15.3
os	4:12	-14.8	-29.0	-45.0	13.5	-16.8	-32.8	-50.9	13.8	-19.1	-37.2	-57.6	15.0
ure	5:12	-14.8	-29.0	-45.1	13.2	-16.8	-32.9	-50.9	13.6	-19.2	-37.3	-57.6	14.9
e C	6:12	-14.9	-29.1	-45.1	13.0	-16.9	-32.9	-50.9	13.5	-19.2	-37.3	-57.7	14.8
ate	7:12	-16.7	-20.2	-20.2	19.3	-18.9	-22.9	-22.9	21.3	-21.5	-26.0	-26.0	23.7
ego	8:12	-16.7	-20.3	-20.3	19.2	-19.0	-23.0	-23.0	21.2	-21.6	-26.1	-26.1	23.6
ory	9:12	-16.8	-20.3	-20.3	19.1	-19.0	-23.0	-23.0	21.1	-21.6	-26.1	-26.1	23.4
D	10:12	-16.8	-20.4	-20.4	19.0	-19.0	-23.0	-23.0	21.0	-21.6		-26.2	23.3
	11:12	-16.8	-20.4	-20.4	18.8	-19.1	-23.1	-23.1	20.9	-21.7	-26.2	-26.2	23.2
	12:12	-16.9	-20.4	-20.4	18.7	-19.1	-23.1	-23.1	20.7	-21.7	-26.2	-26.2	23.1
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	0.7	8.0	1.0	1.1	1.3	1.4	1.9	2.1	2.5	3.2	4.0	4.8
	2:12	1.4	1.4	1.6	1.7	1.9	2.0	2.4	5.6	2.9	3.6	4.3	5.2
	3:12	1.9	1.9	2.0	2.2	2.4	2.5	2.9	3.1	3.4	3.9	4.6	5.5
Do	4:12	2.4	2.4	2.5	2.6	2.8	2.9	3.3	3.5	3.8	4.3	4.9	5.8
owr	5:12	2.8	2.8	2.8	3.0	3.1	3.2	3.7	3.8	4.1	4.6	5.2	6.0
n S	6:12	3.1	3.1	3.1	3.2	3.4	3.5	3.9	4.1	4.3	4.9	5.4	6.2
lop	7:12	3.3	3.3	3.3	3.4	3.6	3.7	4.1	4.3	4.5	5.1	9.5	6.3
е	8:12	3.4	3.4	3.4	3.6	3.7	3.8	4.3	4.4	4.7	5.2	5.7	6.5
	9:12	3.5	3.5	3.6	3.7	3.8	3.9	4.4	4.5	4.8	5.3	5.8	6.5
	10:12	3.6	3.6	3.6	3.8	3.9	4.0	4.4	4.6	4.8	5.3	2.8	9.9
	11:12	3.7	3.7	3.7	3.8	4.0	4.1		4.6	4.9	5.3	5.9	9.9
	12:12	3.7	3.7	3.7	3.9	4.0	4.1	4.5	4.6	4.9	5.3	5.9	6.7

Up and Down (psf)

Side Load (psf)

Lateral

 Ss = 0.0
 Ss = 0.1
 Ss = 0.2
 Ss = 0.3
 Ss = 0.4

 0.0
 0.2
 0.5
 0.7
 0.9

Ss = 0.5 | Ss = 1.0 | Ss = 1.25 | Ss = 1.5 | Ss = 2.0



7:0 ASCE

Mid US (Medium Snow)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

115 mph

25 psf

Basic Wind Speed

Ground Snow Load

Roof Pitch	Up Zone 1	Up Pressures (psf)	one	Down (psf)	Up Zone 1	Up Pressures (pst)	zone 3	Down (psf)	Up Zone 1	Up Pressures (psf) 1 Zone 2 Zone 3	psf) Zone 3	Down (psf)
1:12	-10.8	-20.5	-32.6	25.9	-10.8	-20.5	-32.6	25.9	-13.4	-25.1	-39.8	25.9
2:12	9.6-	-19.3	-30.2	24.6	9.6-	-19.3	-30.2	24.6	-11.9	-23.7	-36.9	24.6
3:12	9.6-	-19.3	-30.2	23.1	9.6-	-19.3	-30.2	23.1	-12.0	-23.7	-36.9	23.1
4:12	-9.7	-19.3	-30.2	21.6	-9.7	-19.3	-30.2	21.6	-12.0	-23.7	-36.9	21.6
5:12	-9.7	-19.4	-30.2	20.1	-9.7	-19.4	-30.2	20.1	-12.0	-23.8	-37.0	20.1
6:12	-9.7	-19.4	-30.3	18.7	-9.7	-19.4	-30.3	18.7	-12.1	-23.8	-37.0	18.7
7:12	-11.0	-13.4	-13.4	18.3	-11.0	-13.4	-13.4	18.3	-13.6	-16.5	-16.5	20.1
8:12	-11.0	-13.4	-13.4	17.2	-11.0	-13.4	-13.4	17.2	-13.6	-16.5	-16.5	18.9
9:12	-11.1	-13.5	-13.5	16.1	-11.1	-13.5	-13.5	16.1	-13.6	-16.6	-16.6	17.9
10:12	-11.1	-13.5	-13.5	15.2	-11.1	-13.5	-13.5	15.2	-13.7	-16.6	-16.6	17.0
11:12	-11.1	-13.6	-13.6	14.4	-11.1	-13.6	-13.6	14.4	-13.7	-16.7	-16.7	16.2
12:12	-11.2	-13.6	-13.6	13.8	-11.2	-13.6	-13.6	13.8	-13.8	-16.7	-16.7	15.9
1:12	-13.4	-25.1	39.8	25.9	-15.6	-29.2	-46.1	25.9	-182	-33.8	-53.4	25.9
2.12	110	73.7	26.0	24.6	14.0	27 E	7.07	24.6	16.2	21.0	40 F	7 7 7
	000	1.02	0.00	0.4.0	2 4	212	42.7	0.4.0	200	0.10	200	
3:17	-12.0	-73./	-30.9	23.1	-14.0	5/7-	1.74-	73.1	-10.3	-31.9	49.5	
4:12	-12.0	-23.7	-36.9	21.6	-14.0	-27.5	-42.8	21.6	-16.3	-32.0	-49.5	
5:12	-12.0	-23.8	-37.0	20.1	-14.0	-27.6	-42.8	20.1	-16.4	-32.0	-49.5	
6:12	-12.1	-23.8	-37.0	18.7	-14.1	-27.6	-42.8	18.7	-16.4	-32.0	-49.6	
7:12	-13.6	-16.5	-16.5	20.1	-15.8	-19.2	-19.2	21.6	-18.4	-22.3	-22.3	
8:12	-13.6	-16.5	-16.5	18.9	-15.9	-19.2	-19.2	20.4	-18.4	-22.3	-22.3	
9:12	-13.6	-16.6	-16.6	17.9	-15.9	-19.3	-19.3	19.4	-18.5	-22.4	-22.4	
10:12	-13.7	-16.6	-16.6	17.0	-15.9	-19.3	-19.3	18.5	-18.5	-22.4	-22.4	
11:12	-13.7	-16.7	-16.7	16.2	-16.0	-19.4	-19.4	18.1	-18.6	-22.5	-22.5	
12:12	-13.8	-16.7	-16.7	15.9	-16.0	-19.4	-19.4	17.9	-18.6		-22.5	
1:12	-16.5	-30.7	-48.5	25.9	-18.7	-34.8	-54.8	25.9	-21.3	-39.4	-62.1	- 1
2:12	-14.7	-29.0	-45.0	24.6	-16.8	-32.8	-50.8	24.9	-19.1	-37.2	-57.5	
3:12	-14.8	-29.0	-45.0	23.1	-16.8	-32.8	-50.8	23.4	-19.1	-37.2	-57.6	- 1
4:12	-14.8	-29.0	-45.0	21.6	-16.8	-32.8	-50.9	21.9	-19.1	-37.2	-57.6	
5:12	-14.8	-29.0	-45.1	20.1	-16.8	-32.9	-50.9	20.4	-19.2	-37.3	-57.6	
6:12	-14.9	-29.1	-45.1	18.7	-16.9	-32.9	-50.9	19.0	-19.2	-37.3	-57.7	
7:12	-16.7	-20.2	-20.2	22.2	-18.9	-22.9	-22.9	23.7	-21.5	-26.0	-26.0	
8:12	-16.7	-20.3	-20.3	21.0	-19.0	-23.0	-23.0	22.5	-21.6	-26.1	-26.1	
9:12	-16.8	-20.3	-20.3	20.0	-19.0	-23.0	-23.0	21.5	-21.6	-26.1	-26.1	
10:12	-16.8	-20.4	-20.4	19.1	-19.0	-23.0	-23.0	21.0	-21.6	-26.2	-26.2	
11:12	-16.8	-20.4	-20.4	18.8	-19.1	-23.1	-23.1	20.9	-21.7	-26.2	-26.2	
12:12	-16.9	-20.4	-20.4	18.7	-19.1	-23.1	-23.1	20.7	-21.7	-26.2	-26.2	
Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
1:12	2.0	2.0	2.0	2.1	2.2	2.3	2.8	5.9	3.2	3.8	4.3	
2:12	3.7	3.7	3.7	3.7	3.7	3.7	4.1	4.3	4.6	5.1	5.7	
3:12	5.0	5.0	5.0	2.0	2.0	5.0	5.2	5.4	5.6	6.2	6.7	
4:12	0.9	6.0	0.9	6.0	0.9	0.9	0.9	6.2	6.4	7.0	7.6	
5:12	6.7	6.7	6.7	6.7	6.7	6.7	6.7	6.7	7.0	7.6	8.1	
6:12	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.1	7.4	7.9	8.4	
7:12	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.5	8.1	8.6	4
8:12	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.6	8.1	8.6	
9:12	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.3	7.5	8.0	8.5	
10:12	7.0	7.0	7.0	7.0	7.0	7.0	7.0	7.1	7.4	7.9	8.4	
11:12	6.8	8.9	8.9	8.9	8.9	8.9	8.9	7.0	7.2	7.7	8.2	
12.12	9	9	2	2	9	9	9	2	!		9	-1
,	1	1	y	9	99	9	6.7	8	7.0	7.5	0 8	

Up and Down (psf)

Side Load (psf)

Lateral

0.2



Massachusetts (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

115 mph

40 psf

Basic Wind Speed

Ground Snow Load

		8	Bldg. Height	= 15	نه	B	Bldg. Height = 30 ft.	ht = 30 f	نبر	B	Bldg. Height	ht = 60 ft.	
	Roof Pitch	Up Zone 1	Up Pressures (psf)	psf) Zone 3	Down (psf)	Up Zone 1	Up Pressures (psf)	osf) Zone 3	Down (psf)	Up Zone 1	Up Pressures (psf)	osf) Zone 3	Down (psf)
	1:12	-10.8	-20.5	-32.6	31.9	-10.8	-20.5	-32.6	31.9	-13.4	-25.1	-39.8	31.9
Е	2:12	9.6-	-19.3	-30.2	30.0	9.6-	-19.3	-30.2	30.0	-11.9	-23.7	-36.9	30.0
Exp	3:12	9.6-	-19.3	-30.2	27.9	9.6-	-19.3	-30.2	27.9	-12.0	-23.7	-36.9	27.9
os	4:12	-9.7	-19.3	-30.2	25.8	-9.7	-19.3	-30.2	25.8	-12.0	-23.7	-36.9	25.8
ure	5:12	-9.7	-19.4	-30.2	23.8	-9.7	-19.4	-30.2	23.8	-12.0	-23.8	-37.0	23.8
e C	6:12	-9.7	-19.4	-30.3	21.9	-9.7	-19.4	-30.3	21.9	-12.1	-23.8	-37.0	21.9
ate	7:12	-11.0	-13.4	-13.4	21.1	-11.0	-13.4	-13.4	21.1	-13.6	-16.5	-16.5	22.8
ego	8:12	-11.0	-13.4	-13.4	19.5	-11.0	-13.4	-13.4	19.5	-13.6	-16.5	-16.5	21.2
ory	9:12	-11.1	-13.5	-13.5	18.1	-11.1	-13.5	-13.5	18.1	-13.6	-16.6	-16.6	19.8
В	10:12	-11.1	-13.5	-13.5	16.9	-11.1	-13.5	-13.5	16.9	-13.7	-16.6	-16.6	18.6
	11:12	-11.1	-13.6	-13.6	15.8	-11.1	-13.6	-13.6	15.8	-13.7	-16.7	-16.7	17.6
	12:12	-11.2	-13.6	-13.6	14.9	-11.2	-13.6	-13.6	14.9	-13.8	-16.7	-16.7	16.7
	1:12	-13.4	-25.1	-39.8	31.9	-15.6	-29.2	-46.1	31.9	-18.2	-33.8	-53.4	31.9
-	2:12	-11.9	-23.7	-36.9	30.0	-14.0	-27.5	-42.7	30.0	-16.3	-31.9	-49.5	30.1
Exp	3:12	-12.0	-23.7	-36.9	27.9	-14.0	-27.5	-42.7	27.9	-16.3	-31.9	-49.5	28.1
008	4:12	-12.0	-23.7	-36.9	25.8	-14.0	-27.5	-42.8	25.8	-16.3	-32.0	-49.5	26.0
sur	5:12	-12.0	-23.8	-37.0	23.8	-14.0	-27.6	-42.8	23.8	-16.4	-32.0	-49.5	23.9
e (6:12	-12.1	-23.8	-37.0	21.9	-14.1	-27.6	-42.8	21.9	-16.4	-32.0	-49.6	22.0
Cat	7:12	-13.6	-16.5	-16.5	22.8	-15.8	-19.2	-19.2	24.3	-18.4	-22.3	-22.3	26.1
eg	8:12	-13.6	-16.5	-16.5	21.2	-15.9	-19.2	-19.2	22.7	-18.4	-22.3	-22.3	24.5
ory	9:12	-13.6	-16.6	-16.6	19.8	-15.9	-19.3	-19.3	21.4	-18.5	-22.4	-22.4	23.1
/ C	10:12	-13.7	-16.6	-16.6	18.6	-15.9	-19.3	-19.3	20.1	-18.5	-22.4	-22.4	21.9
,	11:12	-13.7	-16.7	-16.7	17.6	-16.0	-19.4	-19.4	19.1	-18.6	-22.5	-22.5	20.8
	12:12	-13.8	-16.7	-16.7	16.7	-16.0	-19.4	-19.4	18.2	-18.6		-22.5	20.3
	9	١	100	r of	9	,	3	3	8	:		,	9
	1:12	-16.5	-30.7	-48.5	29.8	-18.7	-34.8	× 4.8	29.8	-21.3		-62.1	29.8
E	2:12	-14./	-29.0	-45.0	28.1	-16.8	-32.8	-50.8	28.4	-19.1	-37.2	-5/.5	29.4
кро	3:12	-14.8	-29.0	-45.0	26.2	-16.8	-32.8	-50.8	26.6	-19.1	-37.2	-57.6	27.5
วรเ	4:12	-14.8	-29.0	-45.0	24.3	-16.8	-32.8	-50.9	24.7	-19.1		-57.6	25.6
ıre	5:12	-14.8	-29.0	-45.1	22.5	-16.8	-32.9	-50.9	22.8	-19.2	-37.3	-57.6	23.8
C	6:12	-14.9	-29.1	-45.1	20.7	-16.9	-32.9	-50.9	21.1	-19.2	-37.3	-57.7	22.0
ate	7:12	-16.7	-20.2	-20.2	24.0	-18.9	-22.9	-22.9	25.5	-21.5	-26.0	-26.0	27.2
ego	8:12	-16.7	-20.3	-20.3	22.5	-19.0	-23.0	-23.0	24.0	-21.6	-26.1	-26.1	25.8
ory	9:12	-16.8	-20.3	-20.3	21.2	-19.0	-23.0	-23.0	22.8	-21.6	-26.1	-26.1	24.5
D	10:12	-16.8	-20.4	-20.4	20.1	-19.0	-23.0	-23.0	21.7	-21.6	-26.2	-26.2	23.4
	11:12	-16.8	-20.4	-20.4	19.2	-19.1	-23.1	-23.1	20.9	-21.7		-26.2	23.2
	12:12	-16.9	-20.4	-20.4	18.7	-19.1	-23.1	-23.1	20.7	-21.7	-26.2	-26.2	23.1
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	5.6	5.6	5.6	2.6	2.7	2.8	3.3	3.4	3.7	4.2	4.8	5.5
	2:12	4.9	4.9	4.9	4.9	4.9	4.9	5.0	5.2	5.5	6.0	9.9	7.2
	3:12	9.9	9.9	9.9	9.9	9.9	9.9	9.9	9.9	6.9	7.4	8.0	9.8
Do	4:12	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	7.9	8.4	9.0	9.6
owi	5:12	8.7	8.7	8.7	8.7	8.7	8.7	8.7	8.7	8.7	9.1	6.7	10.3
n S	6:12	9.5	9.2	9.5	9.5	9.2	9.5	9.5	9.5	9.2	9.5	10.0	10.7
Slo	7:12	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.7	10.2	10.8
ре	8:12	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.4	9.6	10.2	10.8
	9:12	9.5	9.5	9.2	9.5	9.2		9.5	9.5	9.5	9.5	10.0	10.6
	10:12	8.9	8.9	8.9	8.9	8.9		8.9	8.9	6.8	9.3	8.6	10.4
	11:12	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	9.0	9.5	10.0
	12:12	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.2	8.7	9.1	9.7
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
		0	0	0	0	0	,	•	,	0	0		

Up and Down (psf)

Side Load (psf)

Lateral



Mid US (High Snow)*

115 mph

60 psf

Basic Wind Speed

Ground Snow Load

		8	Bldg. Height	= 15	f.	8	Bldg. Height = 30	tht = 30 f	نږ	B :	Bldg. Height	9 =	i.
┪	Roof Pitch	Up Zone 1	Up Pressures (psr)	Zone 3	(psf)	Op Zone 1	Up Pressures (psr)	Zone 3	(psd)	Op Zone 1	Up Pressures (psr)	Zone 3	(psf)
	1:12	-10.8	-20.5	-32.6	45.5	-10.8	-20.5	-32.6	45.5	-13.4	-25.1	-39.8	45.5
E	2:12	9.6-	-19.3	-30.2	41.9	9.6-	-19.3	-30.2	41.9	-11.9	-23.7	-36.9	41.9
хр	3:12	9.6-	-19.3	-30.2	37.8	9.6-	-19.3	-30.2	37.8	-12.0	-23.7	-36.9	37.8
os	4:12	-9.7	-19.3	-30.2	33.6	-9.7	-19.3	-30.2	33.6	-12.0	-23.7	-36.9	33.6
ure	5:12	-9.7	-19.4	-30.2	30.3	-9.7	-19.4	-30.2	30.3	-12.0	-23.8	-37.0	30.3
e C	6:12	-9.7	-19.4	-30.3	27.5	-9.7	-19.4	-30.3	27.5	-12.1	-23.8	-37.0	27.5
at	7:12	-11.0	-13.4	-13.4	25.9	-11.0	-13.4	-13.4	25.9	-13.6	-16.5	-16.5	27.6
eg	8:12	-11.0	-13.4	-13.4	23.5	-11.0	-13.4	-13.4	23.5	-13.6	-16.5	-16.5	25.3
ory	9:12	-11.1	-13.5	-13.5	21.5	-11.1	-13.5	-13.5	21.5	-13.6	-16.6	-16.6	23.3
/ B	10:12	-11.1	-13.5	-13.5	19.7	-11.1	-13.5	-13.5	19.7	-13.7	-16.6	-16.6	21.5
	11:12	-11.1	-13.6	-13.6	18.2	-11.1	-13.6	-13.6	18.2	-13.7	-16.7	-16.7	20.0
	12:12	-11.2	-13.6	-13.6	16.9	-11.2	-13.6	-13.6	16.9	-13.8	-16.7	-16.7	18.7
	1:12	-13.4	-25.1	-39.8	45.5	-15.6	-29.2	-46.1	45.5	-182	-33.8	-53.4	45.5
	2:12	-11.9	-23.7	-36.9	41.9	-14.0	-27.5	-42.7	41.9	-163	-31.9	-49.5	419
Ex	3.12	-120	-23.7	36.9	37.8	-14.0	-275	42.7	37.8	163	31.0	49.5	27.8
рс	31.0	120	7.62-	0.00-	0.70	2.5	27.6	42.0	0.70	16.0	22.0	40.0	0,70
su	21:4	12.0	22.7	-30.9	33.0	14.0	C.12-	42.0	33.0	-10.3	22.0	0.24	33.0
re	2:12	-12.0	-23.8	-3/.0	30.3	-14.0	0.72-	8.74-	30.3	-T0.4	-32.0	0.64	30.4
Ca	6:12	-12.1	-23.8	-37.0	27.5	-14.1	-27.6	42.8	27.5	-16.4		-49.6	27.6
ate	7:17	-13.6	-16.5	-16.5		-15.8	-19.2	-19.2	29.1	-18.4		-77.3	30.9
go	8:12	-13.6	-16.5	-16.5	25.3	-15.9	-19.2	-19.2	26.8	-18.4	-22.3	-22.3	28.6
ory	9:12	-13.6	-16.6	-16.6	23.3	-15.9	-19.3	-19.3	24.8	-18.5	-22.4	-22.4	26.5
С	10:12	-13.7	-16.6	-16.6	21.5	-15.9	-19.3	-19.3	23.0	-18.5	-22.4	-22.4	24.8
	11:12	-13.7	-16.7	-16.7	20.0	-16.0	-19.4	-19.4	21.5	-18.6	-22.5	-22.5	23.2
	12:12	-13.8	-16.7	-16.7	18.7	-16.0	-19.4	-19.4	20.2	-18.6	-22.5	-22.5	21.9
_	1:12	-16.5	-30.7	-48.5	41.4	-18.7	-34.8	-54.8	41.4	-21.3	-39.4	-62.1	41.4
-	2:12	-14.7	-29.0	-45.0	38.0	-16.8	-32.8	-50.8	38.0	-19.1		-57.5	38.0
Exp	3:12	-14.8	-29.0	-45.0	34.4	-16.8	-32.8	-50.8	34.4	-19.1		-57.6	35.2
008	4:12	-14.8	-29.0	-45.0	31.1	-16.8	-32.8	-50.9	31.4	-19.1	-37.2	-57.6	32.4
sur	5:12	-14.8	-29.0	-45.1	28.4	-16.8	-32.9	-50.9	28.7	-19.2	-37.3	-57.6	29.6
e (6:12	-14.9	-29.1	-45.1	25.8	-16.9	-32.9	-50.9	26.1	-19.2	-37.3	-57.7	27.1
Cat	7:12	-16.7	-20.2	-20.2	28.3	-18.9	-22.9	-22.9	29.8	-21.5	-26.0	-26.0	31.5
eg	8:12	-16.7	-20.3	-20.3	26.2	-19.0	-23.0	-23.0	27.7	-21.6	-26.1	-26.1	29.4
ory	9:12	-16.8	-20.3	-20.3	24.3	-19.0	-23.0	-23.0	25.8	-21.6	-26.1	-26.1	27.6
/ D	10:12	-16.8	-20.4	-20.4	22.7	-19.0	-23.0	-23.0	24.2	-21.6	-26.2	-26.2	26.0
	11:12	-16.8	-20.4	-20.4	21.4	-19.1	-23.1	-23.1	22.9	-21.7	-26.2	-26.2	24.6
	12:12	-16.9	-20.4	-20.4	20.2	-19.1	-23.1	-23.1	21.7	-21.7	-26.2	-26.2	23.4
	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	3.8	3.8	4.0	4.6	5.0	5.4	8.9	7.3	8.2	6.6	11.9	14.7
	2:12	7.0	7.0	7.0	7.0	7.4	7.7	9.1	9.6	10.4	12.1	13.8	15.8
	3:12	9.4	9.4	9.4	9.4	9.4	9.6	10.8	11.3	12.1	13.7	15.3	17.2
Do	4:12	11.2	11.2	11.2	11.2	11.2	11.2	12.0	12.5	13.3	14.8	16.3	18.1
wi	5:12	12.3	12.3	12.3	12.3	12.3	12.3	12.8	13.2	13.9	15.3	16.7	18.5
n S	6:12	12.9	12.9	12.9	12.9	12.9	12.9	13.1	13.5	14.1	15.5	16.8	18.4
Slop	7:12	13.1	13.1	13.1	13.1	13.1	13.1	13.1	13.4	14.1	15.3	16.5	18.0
ое	8:12	13.0	13.0	13.0	13.0	13.0	13.0	13.0	13.2	13.7	14.9	16.1	17.5
	9:12	12.6	12.6	12.6	12.6	12.6	12.6	12.6	12.7	13.3	14.3	15.4	16.7
	10:12	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.2	12.7	13.7	14.7	15.9
	11:12	11.4	11.4	11.4	11.4	11.4	11.4	11.4	11.6	12.1	13.0	13.9	15.1
	12:12	10.8	10.8	10.8	10.8	10.8	10.8	10.8	11.0	11.4	12.3	13.2	14.2
		Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
		0	1		•	0	0	0	1	0	·		

Up and Down (psf)

Side Load (psf)

Lateral



7.10 ASCE

APPENDIX - Pressure Tables for Flush Mounted Roof Systems

East Coast (Medium Snow)*

120 mph

25 psf

Basic Wind Speed

Ground Snow Load

ft. Down (psf)	25.9	24.6	23.1	21.6	20.1	18.7	21.0	19.8	18.8	17.9	17.2	17.1	25.9	25.4	23.9	22.3	20.8	19.4	24.5	23.3	22.3	22.1	22.0	21.8	25.9	26.6	25.1	23.6	22.1	20.7	26.8	25.6	25.2	25.1	24.9	Sc = 3.1	5.0	6.3	7.4	8.2	8.8	9.1	9.2	9.2	9.5	9.0	× ×	8.6	Ss = 3.1
= 60	-43.5		-40.3	-40.3	40.4	40.4	-18.1	-18.1	-18.1	-18.2	-18.2	-18.3	-58.2	-54.0	-54.0	-54.0	-54.1	-54.1	-24.4	-24.4	-24.5	-24.5	-24.5	-24.6	-67.7	-62.8	-62.8	-62.8	-62.8	-62.9	-28.4	-28.5	-28.5	-28.6	-28.6			5.7	6.7	9.7	8.1	8.4	9.8	9.8	8.5	8.4	2.2	8.0	Ss = 2.5
Bldg. Height = 60 UpPressures (psf)	-27.5		-25.9	-25.9	-26.0	-26.0	-18.1	-18.1	-18.1	-18.2	-18.2	-18.3	-37.0	-34.8	-34.9	-34.9	-34.9	-35.0	-24.4	-24.4	-24.5	-24.5	-24.5	-24.6	-43.1	-40.6	-40.6	-40.7	-40.7	-40.7	-28.4	-28.5	-28.5	-28.6	-28.6		3.8		6.2	7.0	9.7	7.9	8.1	8.1	8.0	7.9	7.7	7.5	Ss = 2.0
Blo Up i	-14.7	-13.1	-13.1	-13.2	-13.2	-13.2	-14.9	-14.9	-15.0	-15.0	-15.0	-15.1	-20.0	-17.9	-17.9	-17.9	-17.9	-18.0	-20.1	-20.2	-20.2	-20.3	-20.3	-20.3	-23.3	-20.9	-20.9	-20.9	-21.0	-21.0	-23.5	-23.6	-23.6	-23.6	-23.7	Sc = 1.5	3.2	4.6	5.6	6.4	7.0	7.4	7.5	7.6	7.5	7.4	7.2	7.0	Ss = 1.5
t. Down (psf)	25.9	24.6	23.1	21.6	20.1	18.7	19.0	17.9	16.9	16.0	15.2	14.6	25.9	24.6	23.1	21.6	20.1	18.7	22.6	21.4	20.4	19.5	19.4	19.3	25.9	25.6	24.1	22.5	21.0	19.6	24.9	23.7	22.7	22.6	22.3				5.4	6.2	6.7	7.1	7.3	7.3	7.3	7.1	7.0	8.9	Ss = 1.25
Bldg. Height = 30 ft. Jp Pressures (psf) Zone 2 Zone 3	-35.6	-33.0	-33.0	-33.0	-33.0	-33.1	-14.7	-14.7	-14.8	-14.8	-14.8	-14.9	-50.3	-46.6	-46.7	-46.7	-46.7	-46.8	-21.0	-21.0	-21.1	-21.1	-21.2	-21.2	-59.8	-55.4	-55.5	-55.5	-55.5	-55.6	-25.1	-25.1	-25.1	-25.2	-25.2	Sc = 1.0	2.8		5.2	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.9	6.7	Ss = 1.0
Bldg. Height Up Pressures (psf)	-22.4	-21.1	-21.1	-21.2	-21.2	-21.2	-14.7	-14.7	-14.8	-14.8	-14.8	-14.9	-31.9	-30.1	-30.1	-30.1	-30.1	-30.2	-21.0	-21.0	-21.1	-21.1	-21.2	-21.2	-38.0	-35.8	-35.8	-35.9	-35.9	-35.9	-25.1	-25.1	-25.1	-25.2	-25.2	Sc = 0.5	2.3		5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.0	9.9	Ss = 0.5
BI Up Zone 1	-11.9		-10.6	-10.6	-10.7	-10.7	-12.1	-12.1	-12.1	-12.2	-12.2	-12.3	-17.1	-15.3	-15.3	-15.4	-15.4	-15.4	-17.3	-17.4	-17.4	-17.4	-17.5	-17.5	-20.5	-18.4	-18.4	-18.4	-18.4	-18.5	-20.7	-20.7	-20.8	-20.8	-20.9	Sc = 0.4	2.2	3.7	5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.9		Ss = 0.4
t. Down (psf)	25.9	24.6	23.1	21.6	20.1	18.7	19.0	17.9	16.9	16.0	15.2	14.6	25.9	24.6	23.1	21.6	20.1	18.7	21.0	19.8	18.8	17.9	17.2	17.1	25.9	24.6	23.1	21.6	20.1	18.7	23.2	22.1	21.0	20.4	20.3	Sc = 0.3	2.1		5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.0	9.9	Ss = 0.3
Bldg. Height = 15 ft Jp Pressures (psf) Zone 2 Zone 3	-35.6	-33.0	-33.0	-33.0	-33.0	-33.1	-14.7	-14.7	-14.8	-14.8	-14.8	-14.9	-43.5	-40.3	-40.3	-40.3	-40.4	-40.4	-18.1	-18.1	-18.1	-18.2	-18.2	-18.3	-52.9	-49.1	-49.1	-49.1	-49.2	-49.2	-22.1	-22.2	-22.2	-22.3	-22.3	Sc = 0.2	2.0	3.7	5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.0	9.9	Ss = 0.2
BIdg. Height	-22.4	-21.1	-21.1	-21.2	-21.2	-21.2	-14.7	-14.7	-14.8	-14.8	-14.8	-14.9	-27.5	-25.9	-25.9	-25.9	-26.0	-26.0	-18.1	-18.1	-18.1	-18.2	-18.2	-18.3	-33.6	-31.7	-31.7	-31.7	-31.7	-31.8	-22.1	-22.2	-22.2	-22.3	-22.3	Sc = 0.1	2.0	3.7	5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.9	9.9	Ss = 0.1
BI Up Zone 1	-11.9	-10.6	-10.6	-10.6	-10.7	-10.7	-12.1	-12.1	-12.1	-12.2	-12.2	-12.3	-14.7	-13.1	-13.1	-13.2	-13.2	-13.2	-14.9	-14.9	-15.0	-15.0	-15.0	-15.1	-18.1	-16.2	-16.2	-16.2	-16.2	-16.3	-18.3	-18.3	-18.3	-18.4	-18.5	Ss = 0.0	2.0		5.0	0.9	6.7	7.1	7.3	7.3	7.2	7.0	8.9	9.9	Ss = 0.0
Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	12:12	Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	
	Ī	E	хр	os	ure	C	at	eg	ory	/ B				E	Exp	005	sure	e C	Cat	eg	ory	/ C			_		Exp	oos	ure	e C	ate	ego	ory	D		⇈				Do	owi	n S	Slop	ое					

Up and Down (psf)

Side Load (psf)

Lateral

2.9

1.6

0.9

0.7

0.5

0.2



East Coast (Low Snow)*

130 mph

10 psf

Basic Wind Speed

Ground Snow Load

		2	∞		01	_	7	~	_		~	7		2	_	0	-		~	~			-	_	01	2	-		~		~	~	01	_ ,		_												
نہ	(psf)	18.	17.8	17.0	16.2	15.4	14.7	20.2	20.1	20.0	19.8	19.7	19.6	18.	19.9	19.2	18.4	17.6	16.8	25.8	25.6	25.5	25.4	25.3	25.2	18.		20.6	19.8	19.0	18.3	29.3	29.2	29.1	28.0	28.7	Se = 2	4	5.2	5.9	6.4	6.8	7.1	7.2	7.3	7.3	7.7	7.1
9 =	zone 3	-51.2	-47.5	-47.5	-47.5	-47.6	-47.6	-21.4	-21.4	-21.5	-21.5	-21.6	-21.6	-68.5	-63.6	-63.6	-63.6	-63.6	-63.7	-28.8	-28.9	-28.9	-28.9	-29.0	-29.0	-79.7	-73.9	-73.9	-73.9	-74.0	-74.0	-33.6	-33.6	-33.7	-33.7	-33.8	Se = 2 5	4.0	4.5	5.2	5.8	6.2	6.4	9.9	6.7	6.7	9.9	6.5
Bldg. Height = 60	Up Pressures (psf)	-32.5	-30.6	-30.6	-30.7	-30.7	-30.7	-21.4	-21.4	-21.5	-21.5	-21.6	-21.6	-43.6	-41.1	-41.1	-41.2	-41.2	-41.2	-28.8	-28.9	-28.9	-28.9	-29.0	-29.0	-50.7	-47.9	-47.9	-47.9	-48.0	-48.0	-33.6	-33.6	-33.7	-33.7	-33.8	Sc = 20	3.2		4.7	5.2	9.5	5.9	6.1	2.0	6.2	6.1	6.1
8	Up Zone 1	-17.5	-15.6	-15.6	-15.7	-15.7	-15.7	-17.6	-17.7	-17.7	-17.8	-17.8	-17.8	-23.7	-21.2	-21.2	-21.2	-21.3	-21.3	-23.8	-23.9	-23.9	-23.9	-24.0	-24.0	-27.6	-24.7	-24.8	-24.8	-24.8	-24.9	-27.8	-27.8	-27.9	-27.9	-28.0	Ce = 15	2.6	3.4	4.1	4.7	5.1	5.4	5.5	0,0	7.7	2.6	5.6
	(pst)	18.5	17.8	17.0	16.2	15.4	14.7	17.2	17.1	17.0	16.9	16.7	16.6	18.5	18.7	17.9	17.1	16.3	15.6	22.8	22.7	22.5	22.4	22.3	22.2	18.5	20.2	19.4	18.6	17.8	17.0	26.4	26.2	26.1	25.0	25.8	Sc = 1 25	2.3			4.4	4.8	5.1	5.3	4.0	4. P.	4.5	5.4
Bldg. Height = 30 ft	st) Zone 3	-45.0	-38.9	-38.9	-38.9	-39.0	-39.0	-17.4	-17.5	-17.5	-17.5	-17.6	-17.6	-59.3	-55.0	-55.0	-55.0	-55.0	-55.1	-24.8	-24.9	-24.9	-25.0	-25.0	-25.0	-70.4	-65.3	-65.3	-65.3	-65.4	-65.4	-29.6	-29.6	-29.7	7.67-	-29.8	11_	2.1				4.6	4.9		2.5	0.0		
lg. Heigh	Up Pressures (psf)	-26.5	-25.0	-25.0	-25.0	-25.1	-25.1	-17.4	-17.5	-17.5	-17.5	-17.6	-17.6	-37.6	-35.5	-35.5	-35.5	-35.6	-35.6	-24.8	-24.9	-24.9	-25.0	-25.0	-25.0	44.8	-42.2	-42.3	-45.3	-42.3	-42.4	-29.6	-29.6	-29.7	7.67-	-29.8	Cc = 0 5	1.7	2.5		3.8	4.2	4.5	4.7	0.4	φ. 4 0. 4	4.9	6. 4.
B	Up F Zone 1	-14.2	-12.6	-12.7	-12.7	-12.7	-12.8	-14.3	-14.4	-14.4	-14.5	-14.5	-14.5	-20.3	-18.2	-18.2	-18.2	-18.3	-18.3	-20.5	-20.6	-20.6	-20.6	-20.7	-20.7	-24.3		-21.8	-21.8	-21.9	-21.9	-24.5	-24.5	-24.6	24.6	-24.7	Sc = 0.4	1.6		3.1	3.7	4.1	4.4	4.6	/.t	0.4	0 8	4.7
	(pst)	18.5	17.8	17.0	16.2	15.4	14.7	17.2	17.1	17.0	16.9	16.7	16.6	18.5	17.8	17.0	16.2	15.4	14.7	20.2	20.1	20.0	19.8	19.7	19.6	18.5		18.3	17.5	16.7	16.0	23.8	23.7		23.4		Se = 0.3	1.5		3.0	3.6	4.1	4.4	4.6	/.t	4.0	4.7	4.6
Bldg. Height = 15 ft	st) Zone 3	-45.0	-38.9	-38.9	-38.9	-39.0	-39.0	-17.4	-17.5	-17.5	-17.5	-17.6	-17.6	-51.2	-47.5	-47.5	-47.5	-47.6	-47.6	-21.4	-21.4	-21.5	-21.5	-21.6	-21.6	-62.4		-57.8	-57.9	-57.9	-57.9	-26.2	-26.2	-26.2	-26.3	-26.4	Se = 0.2	1.3	2.1	3.0	3.6	4.1	4.4	4.6	/.+ V	4.0	4.7	4.6
dg. Heigh	Up Pressures (pst)	-26.5	-25.0	-25.0	-25.0	-25.1	-25.1	-17.4	-17.5	-17.5	-17.5	-17.6	-17.6	-32.5	-30.6	-30.6	-30.7	-30.7	-30.7	-21.4	-21.4	-21.5	-21.5	-21.6	-21.6	-39.6	-37.4	-37.4	-37.4	-37.4	-37.5	-26.2	-26.2	-26.2	-76.3	-26.4	Se = 0.1	1.1	2.1	3.0	3.6	4.1	4.4	4.6	/.+ V	4.0	4.7	4.6
B	Up F Zone 1	-14.2	-12.6	-12.7	-12.7	-12.7	-12.8	-14.3	-14.4	-14.4	-14.5	-14.5	-14.5	-17.5	-15.6	-15.6	-15.7	-15.7	-15.7	-17.6	-17.7	-17.7	-17.8	-17.8	-17.8	-21.4	-19.2	-19.2	-19.2	-19.3	-19.3	-21.6	-21.7	-21.7	-21.7	-21.8	0 0 = 0 O	1.1		3.0	3.6	4.1	4.4	4.6	4.7	4.0	4.7	4.6
	Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	10:12	11:12	12:12	1:12	2:12	3:12	4:12	5:12	6:12	7:12	8:12	9:12	11:12	12:12	Roof Pitch	1:12	2:12	3:12	4:12	5:12	6:12	7:12	0.12	10:12	11:12	12:12
			E	хр	os	ure) C	at	eg	ory	/ B			_	E	-xp	os	ure	e C	at	eg	ory	С			_	E	- Xp	os	ure	e C	ate	ego	ory	D		╫				Do	lwi	n S	lope	9			

Up and Down (psf

Side Load (psf)

Lateral



New Jersey (Typical)*

130 mph

25 psf

Basic Wind Speed

Ground Snow Load

1.70 2.01	11. 14. 2. 2. 2. 2. 2. 2. 2.			Bld P	leight = 15	ت نے	8 5 ,	Bldg. Height = 30 ft.	ht = 30		_ ,	Bldg. Height = 60	= 60	Down
1112 142 265 462 265 470 265 470 265 470 265 470 265 470 260 1712 414 265 380 246 126 260 470 311 212 212 220 380 211 127 250 389 212 127 250 389 212 127 250 389 212 127 250 389 214 127 250 389 216 127 250 389 216 127 250 389 216 127 250 389 216 127 250 389 216 127 250 389 216 127 390 217 217 217 217 217 217 217 217 217 217 217 217 217 217 217 217 218 217 217 218 217 217 214 217 214 217 </th <th> 11.12 14.2 24.5 </th> <th>Roof</th> <th>1</th> <th>+</th> <th>-1</th> <th>+</th> <th>Zone 1</th> <th>Zone 2</th> <th>Zone 3</th> <th>(bst)</th> <th>Zone 1</th> <th>Zone 2</th> <th>Zone 3</th> <th>(bst)</th>	11.12 14.2 24.5	Roof	1	+	-1	+	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)
212 126 250 389 446 126 250 389 246 126 250 389 246 127 250 389 211 127 250 389 211 127 250 389 211 127 250 389 211 127 250 389 211 127 250 389 211 150 300 407 512 -127 -250 389 216 -127 250 389 216 -157 300 407 512 -127 -250 389 216 -127 250 390 100 -127 200 407 407 612 -128 -178 -176 100 -175 117 -175 117 -175 117 -175 117 -175 117 -175 117 -175 -175 117 -175 -175 -176 -176 -176 -176 -176 -176 <td>212 126 250 389 246 126 306 475 23 412 126 250 389 241 127 250 389 241 127 250 389 216 145 307 475 20 412 -127 -250 389 216 127 -251 390 181 -128 251 307 475 204 417 406 417 206 475 307 475 207 475 174 206 475 307 475 204 417 206 176 217 217 307 475 217 308 417 217 307 475 217 307 475 307 475 317 307 475 307 475 307 475 307 475 307 475 307 476 307 476 307 476 307 477 307 477 307</td> <td>1:1</td> <td>\dashv</td> <td>-</td> <td>\dashv</td> <td>-</td> <td>-14.2</td> <td>-26.5</td> <td>-45.0</td> <td>25.9</td> <td>-17.5</td> <td>-32.5</td> <td>-51.2</td> <td>25.9</td>	212 126 250 389 246 126 306 475 23 412 126 250 389 241 127 250 389 241 127 250 389 216 145 307 475 20 412 -127 -250 389 216 127 -251 390 181 -128 251 307 475 204 417 406 417 206 475 307 475 207 475 174 206 475 307 475 204 417 206 176 217 217 307 475 217 308 417 217 307 475 217 307 475 307 475 317 307 475 307 475 307 475 307 475 307 475 307 476 307 476 307 476 307 477 307 477 307	1:1	\dashv	-	\dashv	-	-14.2	-26.5	-45.0	25.9	-17.5	-32.5	-51.2	25.9
312 12.7 25.0 38.9 21.1 25.0 38.9 21.1 25.0 38.9 21.1 25.0 38.9 21.1 25.0 38.9 21.1 25.1 39.0 21.2 25.1 39.0 21.1 25.1 39.0 21.1 25.1 39.0 21.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 25.1 39.0 11.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 20.1 47.2 40.1 40.2 47.2 47.2 47.2	312 117 250 389 211 115 250 389 121 415 250 447 250 389 121 127 250 389 211 127 251 380 201 115 251 380 201 115 307 476 307 412 123 251 380 201 127 251 389 201 115 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 477 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307 476 307				-38		-12.6	-25.0	-38.9	24.6	-15.6	-30.6		24.6
4.12 1.27 2.50 -38.9 1.16 1.27 2.50 -3.90 1.17 -3.50 -3.70 -4.71 -3.50 -3.71 -3.51 -3.07 -4.71 -3.51 -3.07 -4.71 -3.51 -3.00 -3.71 -3.51 -3.00 -3.71 -3.72<	4.12		+	-	-38	\dashv	-12.7	-25.0	-38.9	23.1	-15.6	-30.6	-47.5	23.1
5112 2121 2321 2300 2011 1127 2511 3900 1001 1557 3900 1001 1557 3000 1001 1557 3000 1001 1557 3000 1001 1557 3000 1001 1100 1100 4000 1100 1001 1100 <th< td=""><td>512 -127 -251 -890 0.01 -128 -251 -390 0.01 -417 -251 -307 -476 -807 -417 -418</td><td></td><td></td><td></td><td>-</td><td></td><td>-12.7</td><td>-25.0</td><td>-38.9</td><td>21.6</td><td>-15.7</td><td>-30.7</td><td>-47.5</td><td>21.6</td></th<>	512 -127 -251 -890 0.01 -128 -251 -390 0.01 -417 -251 -307 -476 -807 -417 -418				-		-12.7	-25.0	-38.9	21.6	-15.7	-30.7	-47.5	21.6
6112 128 251 390 187 128 251 390 187 128 251 390 187 128 251 129 129 1243 124 127 120 121 124 127 120 121 120 124 127 120 121 121 124 127 127 120 121 120 121 120 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 </td <td> Column C</td> <td></td> <td></td> <td>-</td> <td></td> <td>_</td> <td>-12.7</td> <td>-25.1</td> <td>-39.0</td> <td>20.1</td> <td>-15.7</td> <td>-30.7</td> <td>-47.6</td> <td>20.1</td>	Column C			-		_	-12.7	-25.1	-39.0	20.1	-15.7	-30.7	-47.6	20.1
7.12 4.43 4.174 2.06 4.43 4.174 4.104 4.1	7.12 1.43 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.74 -1.75 -1.74 -1.75 -1.74 -1.75 -1.74 -1.75 -1.75 -1.74 -1.75 -				•		-12.8	-25.1	-39.0	18.7	-15.7	-30.7	-47.6	18.7
8.12 1.44 -175 1.94 -175 1.94 -175 -175 1.94 -175 -175 1.94 -177 -175 1.94 -175 -175 1.94 -175 -176 -175 -176 -175 -176 -177 -178 -178 -178 -178 -178 -179 -178 -178 -178 -178 -178 -178 -178 <th< td=""><td>8:12</td><td></td><td></td><td></td><td>_</td><td></td><td>-14.3</td><td>-17.4</td><td>-17.4</td><td>20.6</td><td>-17.6</td><td>-21.4</td><td>-21.4</td><td>22.8</td></th<>	8:12				_		-14.3	-17.4	-17.4	20.6	-17.6	-21.4	-21.4	22.8
9112 144 175 <td>9.12 1.44 1.15 1.16 1.16 1.17 2.15 1.18 1.17 2.15 1.18 2.11 <th< td=""><td></td><td></td><td></td><td></td><td></td><td>-14.4</td><td>-17.5</td><td>-17.5</td><td>19.4</td><td>-17.7</td><td>-21.4</td><td>-21.4</td><td>21.7</td></th<></td>	9.12 1.44 1.15 1.16 1.16 1.17 2.15 1.18 1.17 2.15 1.18 2.11 <th< td=""><td></td><td></td><td></td><td></td><td></td><td>-14.4</td><td>-17.5</td><td>-17.5</td><td>19.4</td><td>-17.7</td><td>-21.4</td><td>-21.4</td><td>21.7</td></th<>						-14.4	-17.5	-17.5	19.4	-17.7	-21.4	-21.4	21.7
10.12 1.45 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.76 1.77 1.77 1.77 1.76 1.76 1.76 1.76 1.77 <t< td=""><td> 10.12 14.5 17.5 17.5 14.5 17.5 </td><td></td><td></td><td>-17</td><td>5 -17.</td><td></td><td>-14.4</td><td>-17.5</td><td>-17.5</td><td>18.4</td><td>-17.7</td><td>-21.5</td><td>-21.5</td><td>20.6</td></t<>	10.12 14.5 17.5 17.5 14.5 17.5			-17	5 -17.		-14.4	-17.5	-17.5	18.4	-17.7	-21.5	-21.5	20.6
11.1.1.2 1.4.5 1.7.6 1.0.6 1.4.5 1.0.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.7.6 1.0.6 1.0.4.5 1.0.7.6 1.0.6 1.0.4.5 1.0.7.6 1.0.6 1.0.4.5 1.0.7.6 1.0.6 1.0.5 1.0.6 1.0.6 1.0.7.6 1.0.6 1.0.7.5 1.0.6 1.0.7.5 1.0.7.6 1.0.7.5 1.0.7.6 1.0.7.5 1.0.7.6 1.0.7.5 1.0.7.6 1.0.7.5 1.0.7.6 1.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7 2.0.7.5 2.0.7	11.1.1.2 1.4.5 1.7.6 1.6.7 1.4.5 1.7.6 1				-17.		-14.5	-17.5	-17.5	17.5	-17.8		-21.5	19.8
1212 1445 176 166 1445 176 166 1445 176 166 1445 176 166 1475 176 166 1475 176 166 1475 176 166 1475 176 166 1475 176 182 235 250 237 243 241 683 2112 -156 306 -47.5 216 -182 355 550 221 241 683 2112 -157 307 -47.6 2116 -183 356 550 212 211 633 5112 -157 307 -47.6 211 -183 356 550 212 211 631 5112 -157 -201 -202 -249 -248 248 248 248 248 248 248 248 248 248 248 248 248 248 248 248 248 248 248 248<	1112 115	11:1				_	-14.5	-17.6	-17.6	16.7	-17.8	-21.6	-21.6	19.7
11.12 11.75 32.5 -21.5 23.5 -23.5 -23.7 -43.6 -43.5 -55.0 25.0 25.9 23.7 -43.6 -43.5 -55.0 25.5 21.1 -43.1 -63.8 21.1 -15.6 -30.6 -47.5 23.1 -18.2 -35.5 -55.0 24.0 -21.2 -41.1 -63.8 21.1 -15.7 -30.7 -47.6 118.7 -35.6 -55.0 21.0 -21.2 -41.1 -63.8 51.1 -15.7 -30.7 -47.6 18.7 -18.3 -35.6 55.0 12.0 -21.2 -41.1 -63.8 61.2 -15.7 -21.4 -21.4 -21.8 -23.6 -55.0 22.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -21.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0 -22.0	11.12 1.15	12:1					-14.5	-17.6	-17.6	16.6	-17.8	-21.6	-21.6	19.6
21.12 1.556 306 -47.5 24.6 -18.2 35.5 55.0 25.2 27.1 41.1 63.8 3.12 -1.56 -306 -47.5 21.4 -18.2 -35.5 -55.0 25.0 21.2 -41.1 63.8 3.12 -1.56 -306 -47.5 21.6 -18.2 -35.5 -55.0 20.2 -21.2 -41.1 63.8 5:1.2 -1.57 -30.7 -47.6 20.1 -18.2 -35.5 -55.0 20.2 -21.2 -41.1 63.8 5:1.2 -1.57 -30.7 -47.6 18.1 -35.6 -55.0 20.1 -11.2 -21.2 -41.2 63.2 -22.2 -21.2 -11.2	2112 156 306 475 214 182 355 550 255 215 411 636 55 55 215 217 411 636 55 217 182 356 550 255 215 217 411 636 55 217 182 350 550 250 250 251 411 636 55 217 182 350 550 250 250 210 213 412 636 25 217 317 307 47.5 18.1 18.2 355 550 250 210 213 412 636 25 217 317 307 47.6 18.7 18.3 356 550 210 213 412 637 20 27 17.1 213 214 214 214 214 214 214 214 214 214 214	=	┢	H	Ľ	Н	-20.3	-37.6	-59.3	25.9	-23.7	-43 6	-68.5	25.9
31.12 1.56 30.6 -47.5 21.8 35.5 55.0 20.0 20.1 -41.2 41.2	3:12 156 306 47.5 21.1 18.2 35.5 55.0 22.0 21.2 41.1 63.6 23.2 41.2 41.2 43.6 23.6 41.2 41.2 41.2 43.6 23.6 41.2 41.2 43.6 23.2 41.2 43.6 23.6 41.2 43.6 23.7 41.2 43.6 23.7 41.2 43.6 23.6 43.2 43.6 23.2 43.6 23.6 23.6 23.0 23.8 28.8 23.8 2			Η.			-18.2	-35.5	-55.0	25.5	-212	-41.1	-63.6	26.7
4:12 4:12 <th< td=""><td>4:12</td><td></td><td>Н</td><td>H.</td><td>H</td><td>H</td><td>-18.2</td><td>-35.5</td><td>55.0</td><td>24.0</td><td>-212</td><td>-41 1</td><td>-63.6</td><td>25.2</td></th<>	4:12		Н	H.	H	H	-18.2	-35.5	55.0	24.0	-212	-41 1	-63.6	25.2
5:12 1:15 307 476 210 1:18 3:56 5:50 2.20 2.21 471 5:00 6:12 1:15 307 476 1:18 3:56 5:50 1:20 2:13 41.2 6:31 6:12 1:15 30.7 47.6 1:18 3:56 5:50 1:20 2:13 41.2 6:33 7:12 1:17 2:14 2:14 2:18 2:06 2:49 2:49 2:49 2:39 2:89 2:89 9:12 1:17 2:14 2:14 2:17 2:06 2:06 2:49 2:49 2:29 2:29 2:89	5.12 15.7 30.7 47.6 20.1 18.3 35.6 55.0 11.0 12.13 41.2 63.6 12.0 12.1 47.6 12.1 18.3 35.6 55.0 11.0 12.13 41.2 63.7 12.0 12.1 12.1 12.1 12.1 12.1 12.1 12.1			+		+	10.1	25.5	200	37.0	21.2	41.2	2000	73.7
6.112	6:12						10.2	25.6	0.00	21.0	21.2	747.2	0.50-	77.67
6:12 -13-7 -30.7 -47.0 18.7 -35.0 -35.1 15.0 -21.3 -35.0 -35.1 15.0 -21.3 -35.0 -35.1 15.0 -21.3 -35.0 -35.	6.12			+	+	+	10.0	0.00	0.00	0.17	C.1.2	717.7	0.00	2.22
7:12 -1.7 -2.14 -2.14 -2.15 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.48 -2.49 -2.49 2.49 2.49 2.49 2.48 -2.48 -2.89 -2.88 9:12 -17.7 -21.6 -21.6 -24.9 -24.9 24.9 23.9 -28.9 -28.8 10:12 -17.8 -21.6 -21.6 -24.9 -24.9 24.9 -23.9 -28.9 -28.2 11:12 -17.8 -21.6 -21.6 -27.0 -25.0 -25.0 -23.9 -28.9 -28.9 11:12 -17.8 -21.6 -21.7 -25.0 -25.0 -27.0 -2	8:12			-		-	-18.3	-35.0	1.55-	19.6	-21.3	7.14-	-63.7	20.8
8:12	8.11		+	_		+	50.5	0.42-	0.42-	24.0	23.0	0.02	0.02-	0.72
9:12	9:17115115115206206249244.9			-			-70.6	6.42-	-24.9	73.6	-23.9	-78.9	6.82-	25.8
1111 1.1. 2 1.1. 3 1.1. 5 1.1. 5 1.1. 5 1.2.	1111 1.1.		+	-	-	-	-20.6	-24.9	-24.9	22.6	-23.9	-28.9	-28.9	25.5
11:11 -17.8 -21.6 -21.6 19.7 -20.7 -25.0 -25.0 22.3 -24.0 -29.0 -29.0 11:12 -17.8 -21.6 -21.6 19.6 -20.7 -25.0 -25.0 -22.2 -24.0 -29.0 -29.0 11:12 -21.4 -39.6 -62.4 25.9 -24.3 -44.8 -70.4 25.9 -24.7 -47.9 -79.2 2:12 -19.2 -37.4 -57.8 25.9 -21.8 42.2 -65.3 27.0 -24.7 -47.9 -73.2 3:12 -19.2 -37.4 -57.8 24.4 -21.8 42.2 -65.3 27.0 -24.7 -79.7 -37.7 -37.8 43.9 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -47.9 -73.2 -37.8 -37.8 -47.9 -73.2<	11:12 -178 -216 -216 19.7 -20.7 -25.0 -25.0 25.3 24.0 -29.0 25.0 25.1 11:12 -178 -216 -21.6 19.6 -20.7 -25.0 -25.0 25.2 24.0 -29.0 25.0		+	-	-	-	-20.6	-25.0	-25.0	22.4	-23.9	-28.9	-28.9	25.4
11.12 -1.16 -2.16 -2.07 -2.50 -2.50 -2.50 -2.90 -2.90 -2.90 -2.90 -2.91 -2.90 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.91 -2.92 -2.91 -4.23 -6.53 2.70 -2.47 -47.9 -79.7 2.112 -19.2 -37.4 -57.8 25.9 -21.8 -42.2 -65.3 27.0 -24.7 -47.9 -73.2 3:12 -19.2 -37.4 -57.9 22.1.8 -42.3 -65.3 25.0 -24.8 -47.9 -73.3 4:12 -19.2 -37.4 -57.9 22.1.8 -42.3 -65.3 25.0 -24.8 -47.9 -73.3 5:12 -19.2 -37.4 -57.9 -21.8 -42.3 -65.3 25.0 -24.8 -47.9 -73.3 5:12 -39.2 -27.9 -27.9 -27.9 -27.	12.12 -17.8 -21.6 -21.6 19.6 -20.7 -25.0 25.0 22.2 -24.0 -29.0 25.0 25.0 22.1 -24.0 -29.0 25.0 25.0 -29.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25	=======================================	+	\dashv	-	-	-20.7	-25.0	-25.0	22.3	-24.0	-29.0	-29.0	25.3
1:12 -214 -396 -62.4 25.9 -24.3 -48.8 -70.4 25.9 -27.6 -50.7 -79.7 2:12 -19.2 -37.4 -57.8 25.9 -21.8 -42.2 -65.3 27.0 -24.7 -47.9 -73.6 3:12 -19.2 -37.4 -57.8 25.9 -21.8 -42.3 -65.3 25.0 -24.8 -47.9 -73.6 4:12 -19.2 -37.4 -57.9 22.9 -21.8 -42.3 -65.3 25.0 -24.8 -47.9 -73.6 5:12 -19.3 -37.4 -57.9 22.9 -21.9 -42.3 -65.4 22.9 -24.8 -47.9 -73.6 -27.0 <td>1:12</td> <td>12:3</td> <td>┨</td> <td>-</td> <td>\dashv</td> <td>\dashv</td> <td>-20.7</td> <td>-25.0</td> <td>-25.0</td> <td>22.2</td> <td>-24.0</td> <td>-29.0</td> <td>-29.0</td> <td>25.2</td>	1:12	12:3	┨	-	\dashv	\dashv	-20.7	-25.0	-25.0	22.2	-24.0	-29.0	-29.0	25.2
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1:12 2.0 2.0 2.0 2.1 2.2 2.3 2.8 2.9 3.2 3.8 2:12 3.7 3.7 3.7 3.7 4.1 4.3 4.6 5.1 3:12 5.0 5.0 5.0 5.0 5.0 5.0 5.2 5.4 4.6 5.1 4:12 6.0 6.0 6.0 6.0 6.0 6.2 6.4 7.0 5:12 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.0 5:12 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.0 7.0 6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.2 7.2 8.1 7:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 8:12 7.2 7.2 7.2 7.2 7.2	1:12 2.0 2.0 2.0 2.1 2.2 2.3 2.8 2.9 3.2 3.8 4.3 5.5 2:12 3.7 3.7 3.7 3.7 3.7 4.1 4.3 4.6 5.1 5.7 6.7 3:12 5.0 5.0 5.0 5.0 5.0 5.2 5.4 5.6 6.7 8.1 8.6 9.3 6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.2 7.2 8.1 8.6 9.3 6:12 6.7 6.7 6.7 6.7	Roof P	Ss	_		Ss=	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss	Ss = 2.0	Ss = 2.5	Ss = 3.3
2:12 3.7 3.7 3.7 3.7 4.1 4.3 4.6 5.1 3:12 5.0 5.0 5.0 5.0 5.0 5.0 5.2 5.4 4.6 5.1 4:12 6.0 6.0 6.0 6.0 6.0 6.0 6.2 6.4 7.0 5:12 6.7 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.0 6:12 7.1 7.2 7.2 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.2 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	2:12 3.7 3.7 3.7 4.1 4.3 4.6 5.1 5.7 6.2 3:12 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 6.2 6.4 5.0 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.6 8.1 8 5:12 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.6 8.1 8 6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.2 8.1 8 9 7:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.2 7.2 7.2 8 9 9 8:12 7.2 7.2 7.2 7.2 7.2 7.2 7.2<	1:1	2.		2.	2.1				5.9			4.3	
3:12 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 6.0 <td>3:12 5.0 5.0 5.0 5.0 5.2 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 6.0<td>2:1</td><td></td><td></td><td></td><td>3.7</td><td>3.7</td><td></td><td></td><td></td><td></td><td>5.1</td><td>5.7</td><td></td></td>	3:12 5.0 5.0 5.0 5.0 5.2 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 6.0 <td>2:1</td> <td></td> <td></td> <td></td> <td>3.7</td> <td>3.7</td> <td></td> <td></td> <td></td> <td></td> <td>5.1</td> <td>5.7</td> <td></td>	2:1				3.7	3.7					5.1	5.7	
4:12 6.0 <td>4:12 6.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 8.4 9 7:12 7.3</td> <td></td> <td>-</td> <td>-</td> <td>-</td> <td>2.0</td> <td>2.0</td> <td>5.0</td> <td>5.2</td> <td>5.4</td> <td>5.6</td> <td>6.2</td> <td>6.7</td> <td>7.4</td>	4:12 6.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 8.4 9 7:12 7.3		-	-	-	2.0	2.0	5.0	5.2	5.4	5.6	6.2	6.7	7.4
5:12 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.6 6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.4 7.9 7:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 8:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 9:12 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 10:12 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 11:12 6.8 6.8 6.8 6.8 6.8 6.7 6.7 6.7 7.5 7.5	5:12 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 7.0 7.0 7.0 8.1 8.1 8.4 9.1 6:12 7.1 7.1 7.1 7.1 7.1 7.2 7.2 8.1 8.4 9.1 7:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 8.6 9.9 8:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.0 8.5 9.9 9:12 7.2 7.2 7.2 7.2 7.3 7.3 7.3 8.0 8.5 9.9 10:12 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 8.4 9. 11:12 6.6 6.6 6.6 6.6 6.6 6.7 6.7 6.7 7.0 7.0 7.0 7.0			-	-	0.9	0.9	0.9	0.9	6.2	6.4	7.0	7.6	8.2
6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.4 7.9 7:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 8.1 8:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 8.1 8.1 9:12 7.2 7.2 7.2 7.2 7.2 7.3 7.3 8.0 10:12 7.0	6:12 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1			_		6.7	6.7	6.7	6.7	6.7	7.0	9.7	8.1	8.
7:12 7.3 7.4 8.1 9:12 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 10:12 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 11:12 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.5 7.5 12:12 6.6 6.6 6.6 6.6 6.6 6.7 6.7 6.7 6.7 7.5 7.5	7:12 7.3 7.4 7.3 8.1 8.6 9 9:12 7.2 7.2 7.2 7.2 7.2 7.3 7.3 7.5 8.0 8.5 9. 10:12 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 8.4 9. 11:12 6.8 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.0 7.1 7.4 7.9 8.2 8. 12:12 6.6 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5 8.2 8. 8 = 0.0 5.8 = 0.0 5.8 = 1.0 5.8 = 1.2 5.8 = 2.0 5.8 = 2.0 5.8 = 2.0 5.8 = 2.0					7.1	7.1	7.1	7.1	7.1	7.4	7.9	8.4	9.1
8:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.5 7.5 8.1 9:12 7.2 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 10:12 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 11:12 6.8 6.8 6.8 6.8 6.8 6.8 6.7 6.7 6.7 7.5	8:12 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.5 8.1 8.6 9.9 9:12 7.2 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 8.5 9. 10:12 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 8.4 9. 11:12 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 8.2 8 12:12 6.6 6.6 6.6 6.6 6.6 6.7 6.7 7.0 7.5 8.2 8 8 8=0.0 5s=0.0 5s=0.1 5s=0.2 5s=0.4 5s=0.5 5s=1.0 5s=1.2 5s=2.0 5s=2.0 5s=2.5 5s=2.5 5s=2.0 5s=2.0 <td></td> <td></td> <td></td> <td></td> <td>7.3</td> <td>7.3</td> <td>7.3</td> <td>7.3</td> <td>7.3</td> <td>7.5</td> <td>8.1</td> <td>9.8</td> <td>9.5</td>					7.3	7.3	7.3	7.3	7.3	7.5	8.1	9.8	9.5
7.2 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 7.0 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5	7.2 7.2 7.2 7.2 7.2 7.2 7.3 7.5 8.0 8.5 9. 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 8.4 9. 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 8.2 8. 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5 8.0 8. 8. 5s=0.0 5s=0.1 5s=0.2 5s=0.3 5s=0.5 5s=1.0 5s=1.2 5s=1.2 5s=2.0 5s=2.5 5s=2.5 5s=2.5			7		7.3	7.3	7.3	7.3	7.3	9.7	8.1	9.8	9.5
7.0 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 6.6 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5	7.0 7.0 7.0 7.0 7.0 7.0 7.1 7.4 7.9 8.4 9. 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 8.2 8.4 9. 6.6 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5 8.0 8. 5s=0.0 5s=0.1 5s=0.2 5s=0.3 5s=0.4 5s=0.5 5s=1.2 5s=1.2 5s=2.0 5s=2.5 5s=2.5 5s=2.5 5s=2.5	9:1	+	-		7.2	7.2	7.2	7.2	7.3	7.5	8.0	8.5	9.5
6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5	6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 7.0 7.2 7.7 8.2 8. 6.6 6.6 6.6 6.7 6.8 7.0 7.5 8.2 8. 8.0 8.0 8.2 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	10:0				7.0	7.0	7.0	7.0	7.1	7.4	7.9	8.4	9.0
6.6 6.6 6.6 6.6 6.6 6.7 6.8 7.0 7.5	6.6 6.6 6.6 6.6 6.7 6.7 6.8 7.0 7.5 8.0 8. Ss=0.0 Ss=0.1 Ss=0.2 Ss=0.4 Ss=0.5 Ss=1.0 Ss=1.2 Ss=1.5 Ss=2.0 Ss=2.5 Ss=2.5 Ss=2.5 Ss=2.6	11:3	+	4	+	8.9	8.9	8.9	8.9	7.0	7.2	7.7	8.2	∞ ∞
	Ss = 0.1 Ss = 0.2 Ss = 0.3 Ss = 0.4 Ss = 0.5 Ss = 1.0 Ss = 1.25 Ss = 1.5 Ss = 2.0 Ss = 2.5 Ss	12:3				9.9	9.9	9.9	6.7	8.9	7.0	7.5	8.0	8.6

Up and Down (psf)

Side Load (psf)

Lateral



7:0 ASCE

Florida (Typical)*
APPENDIX - Pressure Tables for Flush Mounted Roof Systems

160 mph

0 psf

Basic Wind Speed

Ground Snow Load

Up and Down (psf)

Expo	Roof Pitch						iodi comeconi de	1.0					
		Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(Jsd)	Zone 1	Zone 2	Zone 3	(bst)
	1:12	-22.1	-40.8	-64.2	13.4	-22.1	-40.8	-64.2	13.4	-27.1	-49.9	-78.3	13.4
	2:12	-19.8	-38.5	-59.6	15.5	-19.8	-38.5	-59.6	15.5	-24.3	-47.0	-72.6	18.0
	3:12	-19.8	-38.5	-59.6	15.4	-19.8	-38.5	-59.6	15.4	-24.3	-47.1	-72.6	17.9
	4:12	-19.8	-38.6	-59.6	15.3	-19.8	-38.6	-59.6	15.3	-24.4	-47.1	-72.6	17.9
	5:12	-19.9	-38.6	-59.6	15.2	-19.9	-38.6	-59.6	15.2	-24.4	-47.1	-72.7	17.8
	6:12	-19.9	-38.6	-59.7	15.1	-19.9	-38.6	-59.7	15.1	-24.4	-47.1	-72.7	17.6
	7:12	-22.3	-27.0	-27.0	24.4	-22.3	-27.0	-27.0	24.4	-27.3	-33.0	-33.0	28.9
	8:12	-22.3	-27.0	-27.0	24.3	-22.3	-27.0	-27.0	24.3	-27.3	-33.0	-33.0	28.8
	9:12	-22.4	-27.0	-27.0	24.1	-22.4	-27.0	-27.0	24.1	-27.4	-33.1	-33.1	28.6
	10:12	-22.4	-27.1	-27.1	24.0	-22.4	-27.1	-27.1	24.0	-27.4	-33.1	-33.1	28.5
-	11:12	-22.4	-27.1	-27.1	23.9	-22.4	-27.1	-27.1	23.9	-27.5	-33.1	-33.1	28.4
	12:12	-22.5	-27.2	-27.2	23.8	-22.5	-27.2	-27.2	23.8	-27.5	-33.2	-33.2	28.3
	1:12	-27.1	-49.9	-78.3	13.4	-31.5	-57.7	-90.4	13.7	-36.5	-66.7	-104.5	15.2
	2:12	-24.3	-47.0	-72.6	18.0	-28.2	-54.4	-83.9	20.2	-32.7	-62.9	6'96-	22.7
Exp	3:12	-24.3	-47.1	-72.6	17.9	-28.2	-54.4	-83.9	20.1	-32.7	-63.0	-97.0	22.6
	4:12	-24.4	-47.1	-72.6	17.9	-28.3	-54.5	-83.9	20.0	-32.8	-63.0	-97.0	22.5
	5:12	-24.4	-47.1	-72.7	17.8	-28.3	-54.5	-84.0	19.9	-32.8	-63.0	-97.0	22.4
	6:12	-24.4	-47.1	-72.7	17.6	-28.3	-54.5	-84.0	19.8	-32.8	-63.1	-97.0	22.3
	7:12	-27.3	-33.0	-33.0	28.9	-31.6	-38.2	-38.2	32.8	-36.7	-44.2	-44.2	37.3
	8:12	-27.3	-33.0	-33.0	28.8	-31.7	-38.2	-38.2	32.7	-36.7	-44.3	-44.3	37.2
	9:12	-27.4	-33.1	-33.1	28.6	-31.7	-38.3	-38.3	32.6	-36.7	-44.3	-44.3	37.1
	10:12	-27.4	-33.1	-33.1	28.5	-31.8	-38.3	-38.3	32.4	-36.8	-44.3	-44.3	36.9
-	11:12	-27.5	-33.1	-33.1	28.4	-31.8	-38.4	-38.4	32.3	-36.8	-44.4	-44.4	36.8
-	12:12	-27.5	-33.2	-33.2	28.3	-31.8	-38.4	-38.4	32.2	-36.9	-44.4	-44.4	36.7
	1:12	-33.1	-60.7	-95.1	14.2	-37.5	-68.5	-107.3	15.5	-42.5	-77.5	-121.3	17.0
	2:12	-29.7	-57.3	-88.2	21.0	-33.6	-64.6	-99.5	23.2	-38.1	-73.2	-112.6	25.7
	3:12	-29.7	-57.3	-88.3	20.9	-33.6	-64.7	9.66-	23.1	-38.2	-73.2	-112.6	25.6
	4:12	-29.8	-57.3	-88.3	20.9	-33.7	-64.7	9.66-	23.0	-38.2	-73.2	-112.6	25.5
	5:12	-29.8	-57.3	-88.3	20.8	-33.7	-64.7	9.66-	22.9	-38.2	-73.2	-112.7	25.4
C	6:12	-29.8	-57.4	-88.4	20.7	-33.7	-64.8	-99.7	22.8	-38.3	-73.3	-112.7	25.3
	7:12	-33.3	-40.2	-40.2	34.3	-37.7	45.4	45.4	38.2	-42.7	-51.4	-51.4	42.7
	8:12	-33.4	-40.2	-40.2	34.2	-37.7	-45.5	-45.5	38.1	-42.7	-51.5	-51.5	42.6
	9:12	-33.4	-40.3	-40.3	34.1	-37.7	-45.5	-45.5	38.0	-42.8	-51.5	-51.5	42.5
	10:12	-33.4	-40.3	-40.3	33.9	-37.8	-45.5	-45.5	37.8	-42.8	-51.6	-51.6	42.4
-	11:12	-33.5	-40.4	-40.4	33.8		-45.6	-45.6	37.7	-45.8		-51.6	42.2
-	12:12	-33.5	-40.4	-40.4	33.7	-37.9	-45.6	-45.6	37.6	-42.9	-51.6	-51.6	42.1
Ro	Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
	1:12	0.3	9.0	0.8		1.2						4.0	4.8
	2:12	9.0	6.0	1.1	1.3	1.5	1.7	2.3	2.5	2.8	3.6	4.3	5.2
	3:12	6.0	1.2	1.4	1.6	1.8	2.0	2.6	2.8	3.2	3.9	4.6	5.5
	4:12	1.2	1.5	1.7	1.9	2.1	2.3	2.8	3.1	3.4	4.2	4.9	8.8
	6:12		2.0	2.2	2.7	2.6		3 6		3.0	4.6	23	6.0
	7:12	1.9	2.2	2.4	2.6	2.8	2.9			4.1	8.4		6.3
ре	8:12	2.1	2.4	2.6	2.8	3.0	3.1	3.7	3.9	4.2	4.9		6.5
,	9:12	2.3	2.5	2.7	2.9	3.1	3.3	3.8	4.0	4.4	5.0	5.7	6.5
	10:12	2.5	2.7	2.9	3.1	3.3		3.9	4.1	4.5	5.1	5.8	9.9
	11:12	2.6	2.8	3.0	3.2	3.4	3.5	4.0	4.2	4.6	5.2	5.9	9.9
•	71:71	7.7	4	3.T	5.5	5.5	3.0	4.T	4.3	4.0	5.5	S.C	0.7

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Side Load (psf)

Lateral

2.9

0.9

0.7

0.5

0.2



Louisiana (Typical)*

170 mph

0 psf

Basic Wind Speed

Ground Snow Load

Up and Down (psf)

1:12 2:12		Up Pressures (psf)	(Jso	Down	O	Up Pressures (psf)	Jp Pressures (psf)	Down	UD	Up Pressures (psf)	Jo Pressures (psf)	Down
1:12	Zone 1	Zone 2	Zone 3	(bsd)	Zone 1	Zone 2	Zone 3	(bst)	Zone 1	Zone 2	Zone 3	(bst)
2:12	-25.1	-46.3	-72.7	13.4	-25.1	-46.3	-72.7	13.4	-30.8	-56.4	-88.5	13.5
	-22.5	-43.6	-67.4	17.0	-22.5	-43.6	-67.4	17.0	-27.6	-53.3	-82.1	19.8
3:12	-22.5	-43.7	-67.4	16.9	-22.5	-43.7	-67.4	16.9	-27.6	-53.3	-82.1	19.8
4:12	-22.6	-43.7	-67.5	16.9	-22.6	-43.7	-67.5	16.9	-27.6	-53.3	-82.2	19.7
5:12	-22.6	-43.7	-67.5	16.8	-22.6	-43.7	-67.5	16.8	-27.7	-53.3	-82.2	19.6
6:12	-22.6	-43.8	-67.5	16.6	-22.6	-43.8	-67.5	16.6	-27.7	-53.4	-82.2	19.5
7:12	-25.3	-30.6	-30.6	27.1	-25.3	-30.6	-30.6	27.1	-31.0	-37.4	-37.4	32.2
8:12	-25.3	-30.6	-30.6	27.0	-25.3	-30.6	-30.6	27.0	-31.0	-37.4	-37.4	32.1
9:12	-25.4	-30.7	-30.7	8.92	-25.4	-30.7	-30.7	26.8	-31.0	-37.5	-37.5	31.9
10:12	-25.4	-30.7	-30.7	26.7	-25.4	-30.7	-30.7	26.7	-31.1	-37.5	-37.5	31.8
11:12	-25.5	-30.7	-30.7	56.6	-25.5	-30.7	-30.7	56.6	-31.1	-37.5	-37.5	31.7
12:12	-25.5	-30.8	-30.8	26.5	-25.5	-30.8	-30.8	26.5	-31.2	-37.6	-37.6	31.6
1:12	-30.8	-56.4	-88.5	13.5	-35.7	-65.3	-102.3	14.9	-41.4	-75.5	-118.1	16.6
2:12	-27.6	-53.3	-82.1	19.8	-32.0	-61.6	-94.9	22.3	-37.1	-71.2	-109.6	25.1
3:12	-27.6	-53.3	-82.1	19.8	-32.0	-61.6	-94.9	22.2	-37.1	-71.2	-109.6	25.1
4:12	-27.6	-53.3	-82.2	19.7	-32.1	-61.6	-94.9	22.1	-37.2	-71.3	-109.6	25.0
5:12	-27.7	-53.3	-82.2	19.6	-32.1	-61.7	-95.0	22.0	-37.2	-71.3	-109.7	24.9
6:12	-27.7	-53.4	-82.2	19.5	-32.1	-61.7	-95.0	21.9	-37.2	-71.3	-109.7	24.8
7:12	-31.0	-37.4	-37.4	32.2	-35.9	-43.3	-43.3	36.6	-41.5	-50.1	-50.1	41.7
8:12	-31.0	-37.4	-37.4	32.1	-35.9	-43.3	-43.3	36.5	-41.6	-50.1	-50.1	41.6
9:12	-31.0	-37.5	-37.5	31.9	-35.9	-43.3	-43.3	36.4	-41.6	-50.1	-50.1	41.5
10:12	-31.1	-37.5	-37.5	31.8	-36.0	-43.4	-43.4	36.2	-41.7	-50.2	-50.2	41.3
11:12	-31.1	-37.5	-37.5	31.7	-36.0	-43.4	-43.4	36.1	-41.7	-50.2	-50.2	41.2
12:12	-31.2	-37.6	-37.6	31.6	-36.1	-43.5	-43.5	36.0	-41.7	-50.3	-50.3	41.1
1:12	-37.6	-68.7	-107.5	15.5	-42.5	-77.5	-121.3	17.0	-48.1	-87.7	-137.1	18.7
2:12	-33.7	-64.8	-99.8	23.2	-38.1	-73.1	-112.5	25.7	-43.2	-82.8	-127.2	28.5
3:12	-33.7	-64.8	-99.8	23.2	-38.1	-73.2	-112.6	25.6	-43.2	-82.8	-127.3	28.4
4:12	-33.8	-64.9	-99.8	23.1	-38.2	-73.2	-112.6	25.5	-43.3	-82.8	-127.3	28.4
5:12	-33.8	-64.9	-99.9	23.0	-38.2	-73.2	-112.6	25.4	-43.3	-82.8	-127.3	28.3
6:12	-33.8	-64.9	6.66-	22.9	-38.2	-73.3	-112.7	25.3	-43.3	-82.9	-127.4	28.2
7:12	-37.8	-45.5	-45.5	38.3	-42.7	-51.4	-51.4	42.7	-48.3	-58.2	-58.2	47.8
8:12	-37.8	-45.6	-45.6	38.2	-42.7	-51.5	-51.5	42.6	-48.4	-58.2	-58.2	47.7
9:12	-37.8	-45.6	-45.6	38.1	-42.7	-51.5	-51.5	42.5	-48.4	-58.3	-58.3	47.6
10:12	-37.9	-45.6	-45.6	37.9	-42.8	-51.5	-51.5	42.3	-48.4	-58.3	-58.3	47.4
11:12	-37.9	-45.7	-45.7	37.8	-42.8	-51.6	-51.6	42.2	-48.5	-58.4	-58.4	47.3
12:12	-38.0	-45.7	-45.7	37.7	-42.9	-51.6	-51.6	42.1	-48.5	-58.4	-58.4	47.2
Roof Pitch	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1
1:12	0.3	9.0	8.0	1.0	1.2	1.3	1.9	2.1	2.5	3.2	4.0	4.8
2:12	9.0	6.0	1.1	1.3	1.5	1.7	2.3	2.5	2.8	3.6	4.3	5.2
3:12	6.0	1.2	1.4	1.6	1.8	2.0	5.6	2.8	3.2	3.9	4.6	5.5
4:12	1.2	1.5	1.7	1.9	2.1	2.3	2.8	3.1	3.4	4.2	4.9	5.8
5:12	1.5	1.7	1.9	2.2	2.3	2.5	3.1	3.3	3.7	4.4	5.1	6.0
6:12	1.7	2.0	2.2	2.4	5.6	2.7	3.3	3.5	3.9	4.6	5.3	6.2
7:12	1.9	2.2	2.4	2.6	2.8	2.9	3.5	3.7	4.1	4.8	5.5	6.3
8:12	2.1	2.4	5.6	2.8	3.0	3.1	3.7	3.9	4.2	4.9	9.9	6.5
9:12	2.3	2.5	2.7	2.9	3.1	3.3	3.8	4.0	4.4	5.0	5.7	6.5
10:12	2.5	2.7	2.9	3.1	3.3	3.4	3.9	4.1	4.5	5.1	5.8	9.9
11:12	2.6	2.8	3.0	3.2	3.4	3.5	4.0	4.2	4.6	5.2	5.9	9.9
12:12	2.7	2.9	3.1	3.3	3.5	3.6	4.1	4.3	4.6	5.3	5.9	6.7
	Ss = 0.0	Ss = 0.1	Ss = 0.2	Ss = 0.3	Ss = 0.4	Ss = 0.5	Ss = 1.0	Ss = 1.25	Ss = 1.5	Ss = 2.0	Ss = 2.5	Ss = 3.1

Lateral

Side Load (psf)

3.6

0.9

0.7

0.2



APPENDIX C Downward & Upward Span Length Tables

SOLARMOUNT	Standard					Downfo	rce Span	Length				
Rail		20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	12.5 ft	11.0 ft	10.0 ft	9.0 ft	8.5 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.0 ft	4.5 ft
	5 plf	12.5 ft	11.0 ft	10.0 ft	9.0 ft	8.0 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.0 ft	4.5 ft
	10 plf	11.0 ft	10.0 ft	9.0 ft	8.5 ft	8.0 ft	7.5 ft	7.0 ft	6.5 ft	5.5 ft	5.0 ft	4.5 ft
	15 plf	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft
	20 plf	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.0 ft	4.5 ft
Horizontal	25 plf	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft
Load	30 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft
	35 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft
	40 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft
	50 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft
	60 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft

SOLARMOUNT	Standard					Uplif	t Span Ler	ngth				
Rail		20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	12.5 ft	11.0 ft	10.0 ft	9.0 ft	8.5 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.0 ft	4.0 ft
	5 plf	12.5 ft	11.0 ft	10.0 ft	9.0 ft	8.0 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.0 ft	4.0 ft
	10 plf	11.0 ft	10.0 ft	9.0 ft	8.5 ft	8.0 ft	7.5 ft	7.0 ft	6.5 ft	5.5 ft	5.0 ft	4.0 ft
	15 plf	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.0 ft
	20 plf	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.0 ft	4.0 ft
Horizontal	25 plf	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.0 ft
Load	30 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft
	35 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft
	40 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft
	50 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft
	60 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft

Note: No Interpolation Permitted.

Example:

Downward Load (strong axis) 60 plf 50 plf Upward Load (strong axis) 10 plf Horizontal Load (weak axis)

8.0 ft Max Span for Downforce 8.5 ft Max Span for Uplift 8.0 ft

Max Span = min (downforce, uplift) with SOLARMOUNT Standard Rail



APPENDIX C Downward & Upward Span Length Tables

SOLARMOUN	IT Light					Downfo	rce Span	Length				
(LT) Ra	il	20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	8.0 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.5 ft	3.0 ft
	5 plf	8.0 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.5 ft	3.0 ft
	10 plf	7.5 ft	7.0 ft	6.0 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.5 ft	3.0 ft
	15 plf	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	3.0 ft
	20 plf	6.0 ft	5.5 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	3.0 ft
Horizontal	25 plf	5.5 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	4.0 ft	3.5 ft	3.0 ft	3.0 ft
Load	30 plf	4.5 ft	4.0 ft	4.0 ft	3.5 ft	3.5 ft	3.0 ft	3.0 ft				
	35 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.0 ft	3.0 ft					
	40 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft					
	50 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft					
	60 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft					
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft					

SOLARMOUN	IT Light	Uplift Span Length										
(LT) Ra	il	20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	8.0 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
	5 plf	8.0 ft	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
	10 plf	7.5 ft	7.0 ft	6.0 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
	15 plf	7.0 ft	6.5 ft	6.0 ft	5.5 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
	20 plf	6.0 ft	5.5 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
Horizontal	25 plf	5.5 ft	5.5 ft	5.0 ft	5.0 ft	4.5 ft	4.5 ft	4.0 ft	4.0 ft	3.5 ft	3.0 ft	2.5 ft
Load	30 plf	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.0 ft	4.0 ft	3.5 ft	3.5 ft	3.0 ft	2.5 ft
	35 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.0 ft	2.5 ft
	40 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	2.5 ft
	50 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft
	60 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft

Note: No Interpolation Permitted.

Example:

60 plf Downward Load (strong axis) 50 plf Upward Load (strong axis) Horizontal Load (weak axis)

5.0 ft Max Span for Downforce 5.5 ft Max Span for Uplift 5.0 ft

Max Span = min (downforce, uplift) with SOLARMOUNT Light (LT) Rail



APPENDIX C Downward & Upward Span Length Tables

SOLARMOUN	T Heavy	Downforce Span					rce Span	Length				
Duty (HD)	Rail	20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	18.5 ft	16.0 ft	14.5 ft	13.5 ft	12.5 ft	12.0 ft	11.5 ft	10.5 ft	9.0 ft	7.0 ft	6.0 ft
	5 plf	18.5 ft	16.0 ft	14.5 ft	13.5 ft	12.5 ft	12.0 ft	11.5 ft	10.0 ft	9.0 ft	7.0 ft	6.0 ft
	10 plf	11.5 ft	11.5 ft	11.5 ft	11.5 ft	11.5 ft	11.5 ft	11.0 ft	10.0 ft	9.0 ft	7.0 ft	6.0 ft
	15 plf	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.0 ft	6.0 ft
	20 plf	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft
Horizontal	25 plf	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft
Load	30 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft
	35 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft
	40 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft
	50 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft
	60 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft

SOLARMOUN	T Heavy	Uplift Span Length										
Duty (HD)	Rail	20 plf	30 plf	40 plf	50 plf	60 plf	70 plf	80 plf	100 plf	120 plf	150 plf	180 plf
	0 plf	18.5 ft	16.0 ft	14.5 ft	13.5 ft	12.5 ft	10.5 ft	9.0 ft	7.5 ft	6.0 ft	5.0 ft	4.0 ft
	5 plf	18.5 ft	16.0 ft	14.5 ft	13.5 ft	12.5 ft	10.5 ft	9.0 ft	7.5 ft	6.0 ft	5.0 ft	4.0 ft
	10 plf	11.5 ft	11.5 ft	14.0 ft	13.0 ft	12.0 ft	10.5 ft	9.0 ft	7.5 ft	6.0 ft	5.0 ft	4.0 ft
	15 plf	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	7.5 ft	9.0 ft	7.5 ft	6.0 ft	5.0 ft	4.0 ft
	20 plf	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	5.5 ft	6.0 ft	5.0 ft	4.0 ft
Horizontal	25 plf	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.5 ft	4.0 ft
Load	30 plf	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft	3.5 ft
	35 plf	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft	3.0 ft
	40 plf	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft	2.5 ft
	50 plf	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft	2.0 ft
	60 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft
	70 plf	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft	1.5 ft

Note: No Interpolation Permitted.

Example:

60 plf Downward Load (strong axis) 50 plf Upward Load (strong axis) Horizontal Load (weak axis)

11.5 ft Max Span for Downforce 13.0 ft Max Span for Uplift 11.5 ft Max Span = min (downforce, uplift)

with SOLARMOUNT Heavy Duty (HD) Rail



SOLARMOUNT FRONT TRIM

SOLARMOUNT Front Trim should not be installed in areas where the wind load exceeds 100 psf, where the distance from clamp to clamp (span) exceeds 52 inches, or where the cantilever (overhang) is greater than 66% of the span length.





Roof Pitch to Angle Conversion:

$$12:12 = 45^{\circ}$$

$$9:12 = 36.87^{\circ}$$

$$7:12 = 30.26^{\circ}$$

$$6:12 = 26.57^{\circ}$$

$$5:12 = 22.62^{\circ}$$

Still Walkable

Standard Roof Pitch

$$3:12 = 14.04^{\circ}$$

Typical in Southern Climates

$$2:12 = 9.46^{\circ}$$

Low Roof Pitch





The Pressure Lookup Tables and U-Builder include service dead loads ranging from 2.1 to 3.8 psf and include the weight of SOLARMOUNT Standard Rail, SOLARMOUNT connections, and the weight of the module.

To calculate the dead load of your system, please refer to Appendix G - Technical Data Sheet and the project specific Module Specification Sheet. If your loads fall outside the range listed above, please use the Analytical Method in the SOLARMOUNT Design and Engineering Guide for analysis.



e]enphase

Fault Test Parameters

Installation Parameters for Equipment Grounding Fault Test

Enphase Energy is looking to perform fault testing to verify that our microinverter enclosure and cabling system can be utilized to clear a 20A fault condition occurring on the metallic racking or module frames components. These bonding devices can be either WEEB grounding clips or UL-2703 listed bonding within a system in which all of the metallic equipment is bonded using devices listed for bonding the components, but the primary test scenario is designed to utilize WEEB grounding clips.

Installation Parameters

Ideally, we would like to show that a single microinverter can clear a fault condition occurring on the second rail of the racking system. WEEB grounding clips would be used for bonding the modules, microinverters, and racking system. WEEB DMC clips with Unitac SolarMount Rails would be an acceptable pairing. The wire length between the microinverter and the overcurrent protective device should be maintained to at least 2% voltage drop, but 3% voltage drop (based upon 16A) would be ideal.

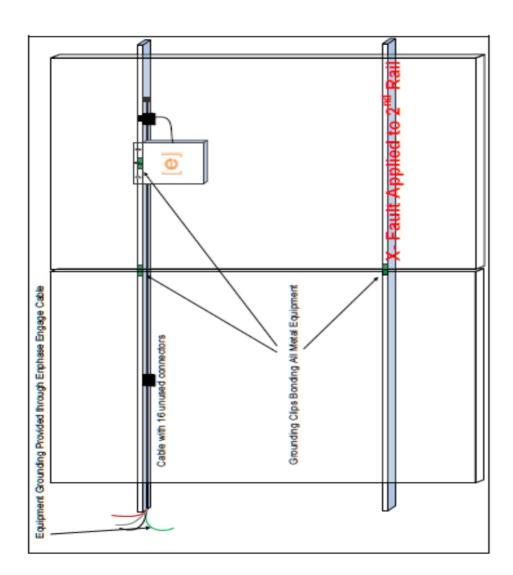
If the primary test scenario is adequate to properly open the breaker, then no additional testing would be

Primary Test Scenio - One Inverter to clear fault, 3% voltage drop

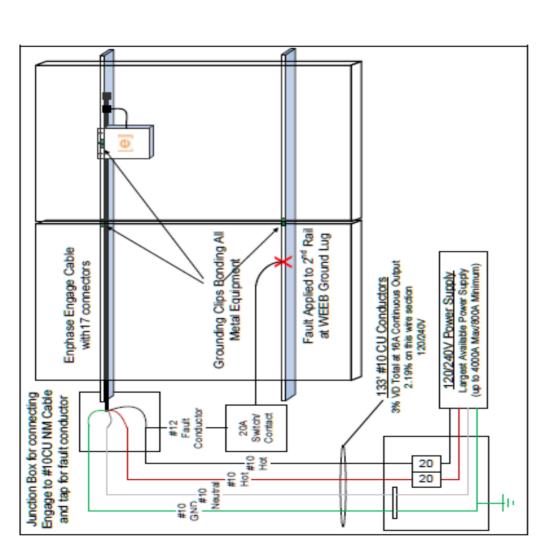
Installation Requirements for the primary test scenario

- 2 modules (could be used Sharp 235s from Enphase inventory)
- 2 rail 2 x 8' sections of Unirac U-SMR Rail
- Flat-lid microinverter (M215 and/or M250 acceptable)
- WEEB-DMC grounding clips between metal components and installed as per Burndy installation requirements
- WEEB Grounding Lug for bonding of fault to 2rd rail
- Enphase Engage Cable with 17 portrait connectors in portrait (.81% voltage drop when fully populated. The microinverter is to be installed at the 17th connector in the cable
- 81% on Engage Cable with 17 portrait connectors (from Enphase Vrise Technical Brief) 2.19% voltage drop on #10 conductors
- Designed for 3% Voltage Drop total including Engage Cable of #10 CU conductors
- 133' of #10 CU conductors Could be type NM cable.
- Vdrop % = 16A x 2 way wire length in kFt x Resistance Ω/kFt / 240V
 - 2.19% = 16A x 2 x Distance x 1.24D/KR / 240V
 - One Way Distance of #10CU = 133 ft
- Fault applied to 2" rail
- Bonding of modules to rail with 1 WEEB clip per mid clamp
 - Bonding of microinverter to rail with 1 WEEB clip

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Electrical Schematic



Other Potential Test Scenarios

Additional test scenarios may be required or preferred. Alternate test parameters may include the following:

- We may want to test both M215 and M250 microinverters
- Decreasing Voltage Drop from 3% to 2% with use of 72' one way wire length of #100U conductors
 - Apply fault to module frame
 - Apply fault to 1st rail
- Install 2 or more microinverters on the cable / rail section
- Use UL-2703 racking system in place of WEEB bonding clips (potentially Unirac rail-less system) Test with approved Siemens AFCI Breaker

141-001NS Rev 00

Equipment Grounding in an Enphase System

e]enphase

Brief

Technical

Overview

and less prone to the fire hazards that come with higher voltage DC photovoltaic systems. Many of these Microinverter system provides a system that is safer for service personnel, safer for fire fighter personnel The Enphase An Enphase Energy Microinverter system offers the safest photovoltaic system available. safety advantages are widely known:

- DC voltages are maintained at low, safe levels
- Conduits and conductors are de-energized when the main breaker is shut-off.
- Enphase Microinverter systems are free of DC arc-fault hazards and requirements

However, one advantage that is rarely discussed is the high levels of ground bonding that exists in an Enphase Microinverter system.

and when properly bonded to racking and to modules frames provides for robust equipment grounding to this equipment, also. When the microinverters, racking, and modules are properly bonded together, then the equipment grounding may also be provided through the microinverter. This can provide a significant Each and every microinverter in an Enphase system is bonded to ground through the Enphase Engage cabling system. The Enphase Engage cable provides for a robust grounding path to each microinverter cost savings to the labor and balance of system costs in an Enphase Microinverter system.

Enphase Grounding and the 2011 National Electrical Code

Equipment Grounding and System Grounding Requirements

Systems that meet the The Enphase M250-IG and M215-60-2LL-S22-IG meet the requirements of the National Electrical Code Article 690.35 Ungrounded Photovoltaic Power Systems. NEC 690.35 allows for photovoltaic power requirements of NEC 690.35 are exempt from the requirements of NEC 690.41 System Grounding. systems to be installed with ungrounded photovoltaic source and output circuits.

DC conductors are not bonded to ground and the microinverters do not require a GEC, but do require that grounding requires the installation of a grounding electrode conductor (GEC). In an Enphase system, the grounding path between a grounding electrode (I.E. ground rod or ufer) and a grounded system. System Equipment grounding provides for the grounding of metal equipment and enclosures and is generally provided for with equipment grounding conductors (EGCs). System grounding provides the primary The NEC calls out two distinct types of grounding; equipment grounding and system grounding. EGCs are provided for equipment grounding.

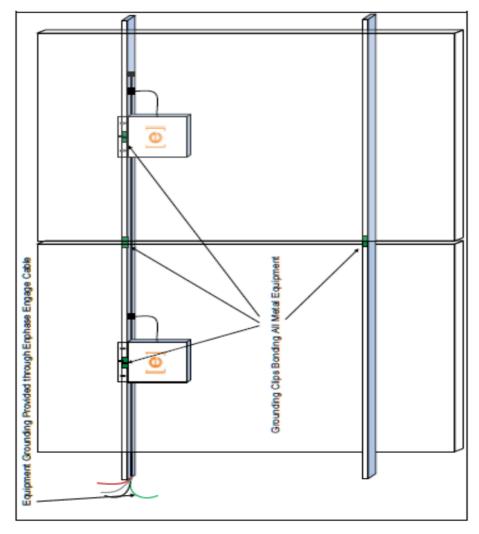
required to have equipment grounding provided to the metal frames, equipment, and enclosures in the grounding electrode conductor (GEC) is not required to be installed to the enclosure of each Enphase The tern ungrounded is somewhat misleading, because ungrounded photovoltaic systems are still system, but are not required to meet the requirements for system grounding. This means that a Microinverter Systems that do band the DC conductors of the photovoltaic source and output circuits must meet the installation requirements for the grounding electrode conductors (GEC) as called out in NEC 250.64, which requires that the GEC be continuous and protected against damage. The grounding electrode conductor (GEC) must also be a minimum #8CU conductor, as required by NEC 250.166.

PAGE F4

NEC Article 690.43 Equipment Grounding specifies that all exposed non-current-carrying metal parts of PV module frames, electrical equipment, and conductor enclosures shall be provided with equipment grounding.

grounding the metallic frames of PV modules or other equipment shall be permitted to bond the exposed 690.43(C) Structure as Equipment Grounding Conductor allows for equipment to be used as the equipment grounding conductor in a photovoltaic system. Specifically, "Devices listed and identified for metal surfaces or other equipment to mounting surfaces.

In an Enphase microinverter system, if the microinverters and modules are bonded to the racking assemblies with the use of listed and approved grounding clips or grounding components, then the equipment grounding conductor provided to the microinverters through the Enphase Engage cable may also be used to ground the other photovoltaic system components.



**Always check with your Authority Having Jurisdiction about your proposed grounding methodology prior to the installation of the system.

APPENDIX F **Enphase Energy Microinverter Testing**



Enphase microinverters meet the requirements of NEC Article 690.35 for Ungrounded Photovoltaic Power

Meeting the Requirements of NEC 690.35 Ungrounded Photovoltaic Power Systems

690.35 Ungrounded Photovoltaic Power Systems. Photovoltaic Power Systems shall be permitted to operate with ungrounded photovoltaic source and output circuits where the system complies with 890.35(A) through (G).

(A) Disconnects. In an Enphase microinverter system the AC and DC connectors are the disconnecting means.

Overcurrent Protection. In an Enphase system, the AC circuit breaker or fused disconnecting feeding the branch circuit provides overcurrent protection for the inverter output circuit. As per 690.9(A) Exception (b), overcurrent protection is not required on the DC conductors. <u>@</u>

provided in the microinverter. In the Enphase microinverters with integraled grounding, the Ground Fault Protection. In an Enphase microinverter system, ground fault protection is ground fault protection is provided by a ground fault sensing circuit. Q

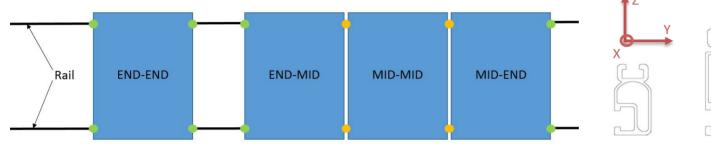
The DC conductors must be PV Wire. The DC conductors in an Enphase Microinverter are PV 0

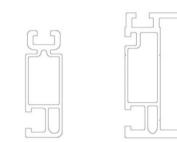
(E) Allowed for use in ungrounded battery systems
 (F) Labelling. The Enphase Microinverters are labeled as specified.
 (G) Listing. The Enphase Microinverters are listed for use in an ungrounded photovoltaic system.





Midclamp and Endclamp Loads per Module





Module Condition Definitions:

END-END: The END-END module shown above, correlating with the loads below, indicates a module that is secured by 4 Endclamps on 2 rails. **END-MID/MID-END**: The END-MID and MID-END modules shown above, correlating with the loads below, indicate modules that are secured by 2 Endclamps and 2 Midclamps on 2 rails.

MID-MID: The MID-MID module shown above, correlating with the loads below, indicate a module that is properly secured by 4 Midclamps on 2 rail

	Middamp and Enddamp Loads per Module												
		Allowable Load (lbs)					Design Load (Ibs)						
	Loading Condition (with	Standard Clamps			Pro-Series Clamps			Standard Clamps			Pro-Series Clamps		
Rail	Respect to Rail)	End-End	End-Mid & Mid-End	Mid-Mid	End-End	End-Mid & Mid-End	Mid-Mid	End-End	End-Mid & Mid-End	Mid-Mid	End-End	End-Mid & Mid-End	Mid-Mid
	Z+, Tension	1836	1801	1766	1064	1510	1956	2780	2726	2672	1724	2342	2960
SM/SM HD	Y±, Transverse*	178*	315*	428	288	392	468	269*	476*	647	436	594	708
GIVI/ GIVI TID	X±, Sliding	244	244	850	2238	356	710	368	368	1286	3136	538	1074
	Y±, Transverse w/33mm Module	67	248	428	288	392	468	102	373	647	436	594	708
	Z+, Tension	1260	1234	1208	1064	1235	1406	1908	1867	1826	1724	1925	2126
SM LT	Y±, Transverse*	139*	225*	419	288	378	468	211*	340*	634	436	594	708
GWI LI	X±, Sliding	266	266	840	2238	356	710	402	402	1270	3136	538	1074
	Y±, Transverse w/33mm Module	67	225	419	288	378	468	102	340	634	436	594	708

^{*}For transverse loads associated with using "C" Endclamps and 33 mm Modules, please see "Y±, Transverse w/33mm Module'

Midclamp: Part No. - 302030M, 302030D. Material - 6000 Series Aluminum Alloys. Ultimate Tensile Strength - 38 ksi. Yield Strength - 35 ksi. Finish - Black Anodize or Mill. Weight ~ 0.097 lbs (50 g)

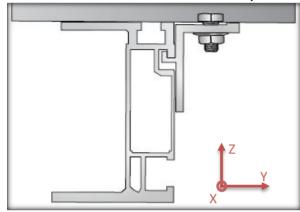
Endclamp: Part No. - 302040M. Material - 6000 Series Aluminum Alloys. Ultimate Tensile Strength - 38 ksi. Yield Strength - 35 ksi. Finish - Mill. Weight ~ 0.124 lbs (57 g)

^{***}NOTE: See NOTES on Page G2.





SOLARMOUNT BOTTOM MOUNTING CLIP (SM HD ONLY)



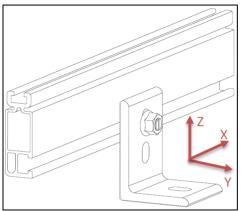
Bottom Mounting Clip (SM HD Only)						
	Allowable					
Direction	Load (Ibs)	Load (Ibs)				
	SM HD	SM HD				
X±, Sliding	27	41				
Y±, Transverse	329	497				
Z+, Tension	686	746				

Part No. 302000C

Bottom Mounting Clip Material: 6000 Series Aluminum Alloys Ultimate Tensile Strength: 38 ksi, Yield Strength: 35 ksi

Finish: Clear Anodized

SOLARMOUNT L-FOOT



L-Foot with 3/8" T-Bolt								
Direction	Allowable	Load (Ibs)	Design L	oad (Ibs)				
Direction	SM/SM HD	SMLT	SM/SM HD	SMLT				
X±, Sliding	565	594	854	898				
Y±, Transverse	146	172	220	261				
Z+, Tension	938	603	1419	911				

Part No. 304001C, 304001D

1357

L-Foot material: 6000 Series Aluminum Alloys

1297

2052

1962

Ultimate Tensile: 38 ksi, Yield: 35 ksi Finish: Clear or Dark Anodized L-Foot Weight: 0.215 lbs (98q)

NOTES:

Allowable and design loads are valid when components are assembled according to authorized UNIRAC documents.

For the beam to L-Foot connection: Assemble with one Unirac 3/8"-20 T-Bolt and one 3/8"-20 ASTM F594 serrated flange nut.

Use anti-seize and torque the Midclamp, Endclamp, and Bottom Mounting Clip to 10 ft-lbs. Use anti-seize and torque the L-Foot to 30 ft-lbs.

Values for the L-Foot and Bottom Mounting Clip represent the capacity of a single part when used with a SOLARMOUNT series rail to retain a module in the direction indicated.

2

Z-, Compression

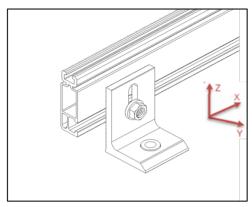
Assemble Midclamp and Endclamp with one Unirac 1/4"-20 T-Bolt and one 1/4"-20 ASTM F594 serrated flange nut.

SM = SOLARMOUNT Standard Rail, SM HD = SOLARMOUNT Heavy Duty Rail, SM LT = SOLARMOUNT Light Rail





FLASHKIT PRO L-FOOT



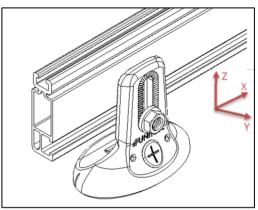
L-foot with 3/8" T-Bolt							
Direction	Allowable L	oad (lbs)	Design Load (lbs)				
Direction	SM/SM HD	SMLT	SM/SM HD	SMLT			
X±, Sliding	589	419	892	634			
Y±, Transverse	175	208	266	316			
Z+, Tension 824		650	1246	983			
Z-, Compression	1540	1525	2330	2307			

Part no. 004055M, 004055D

Flashkit Pro L-Foot Material: 6000 Series Aluminum Alloys Ultimate Tensile Strength: 38 ksi, Yield Strength: 35 ksi

Finish: Mill or Dark Anodized Weight: 0.215 lbs (98 g)

FLASHLOC COMP MOUNT



Flashloc Comp Mount with 3/8" T-Bolt						
Direction	Allowable I	_oad (lbs)	Design Load (lbs)			
Direction	SM/SM HD	SMLT	SM/SM HD	SMLT		
X±, Sliding	584	573	884	866		
Y±, Transverse	162	172	246	261		
Z+, Tension	483	420	483	420		
Z-, Compression	629	468	629	468		

Part no. 004085M, 004085D

Flashloc Comp Mount Material: A380 Cast Aluminum Ultimate Tensile Strength: 46 ksi, Yield Strength: 23 ksi

Finish: Mill or Black E-coat Weight: 0.295 lbs (134 g)

NOTES:

Allowable and design loads are valid when components are assembled according to authorized UNIRAC documents.

For the beam to L-Foot connection: Assemble with one Unirac ³/₈"-20 T-Bolt and one ³/₈"-20 ASTM F594 serrated flange nut.

Use anti-seize and torque the Midclamp, Endclamp, and Bottom Mounting Clip to 10 ft-lbs. Use anti-seize and torque the L-Foot to 30 ft-lbs. values

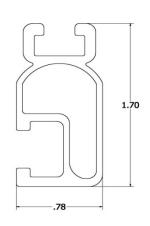
for the

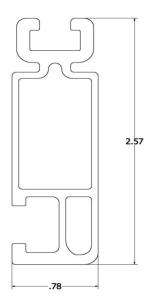
Assemble Midclamp and Endclamp with one Unirac ½"-20 T-Bolt and one ½"-20 ASTM F594 serrated flange nut. SM = SOLARMOUNT Standard Rail, SM HD = SOLARMOUNT Heavy Duty Rail, SM LT = SOLARMOUNT Light Rail

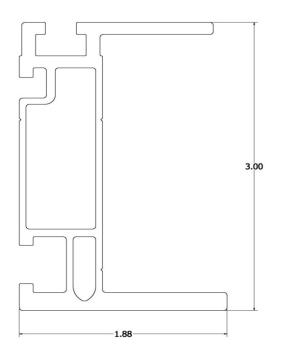




Material: 6000 Series Aluminum Alloys Ultimate Tensile: 38 ksi, Yield: 35 ksi Finish: Mill, Clear or Dark Anodized





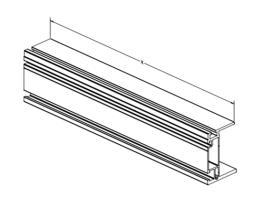


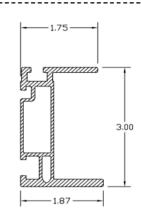
Properties	SOLARMOUNT Light	SOLARMOUNT Rail Profile 2	SOLARMOUNT HD	Units
BEAM HEIGHT	1.70	2.57	3.00	in
APPROX WEIGHT	0.491	0.728	1.271	plf
CROSS SECTION AREA	0.409	0.625	1.059	in²
SECTION MODULUS (X-AXIS)	0.15	0.363	0.898	in³
SECTION MODULUS (Y-AXIS)	0.067	0.113	0.221	in³
MOMENT OF INERTIA (X-AXIS)	0.13	0.467	1.45	in ⁴
MOMENT OF INERTIA (Y-AXIS)	0.026	0.045	0.267	in ⁴
RADIUS OF GYRATION (X-AXIS)	0.564	0.865	1.17	in
RADIUS OF GYRATION (Y-AXIS)	0.254	0.269	0.502	in

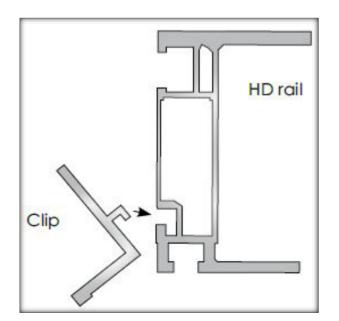




The SOLARMOUNT Installation Guide and system certifications are equally applicable to SOLARMOUNT HD and Light rail. Unless otherwise noted, installation procedures for both are equivalent and sufficient to maintain system certifications. For maximum spans and cantilevers specific to SOLARMOUNT HD and Light rail, please refer to Appendix C and the SOLARMOUNT Installation Guide.







Bottom Mounting with SOLARMOUNT HD Rail:

Bottom mounting is no longer possible with standard SOLARMOUNT or Light rail, however, SOLARMOUNT HD still accommodates this mounting method. Should you elect to use bottom mounting clips to secure modules, please refer to the procedure below. NOTE: Bottom mounting of modules does not provide module bonding through clips and is not covered under the current UL 2703 certification.

	Wrench size	* Recommended torque (ft-lbs)	
¼" hardware 3%" hardware	7/16" 9/16"	10 30	

Note:Torque specifications do not apply to lag bolt connections.



Stainless steel hardware can seize up, a process called galling. To significantly reduce its likelihood, (1) apply lubricant to bolts, preferably an anti-seize lubricant, available at auto parts stores, (2) shade hardware prior to installation, and (3) avoid spinning on nuts at high speed. See Installation Supplement 910, Galling and Its Prevention, at www.unirac.com.

^{*}With anti-seize





Flashkit Pro L-Foot

	for SM Standard (ft.)/Maximum Reaction Force (lbs)						
	At	tachment Spaci	ng				
ΔΤ (°F)	24"	48"	72"				
40	59/133	86/193	105/236				
50	55/155	70/197	93/262				
60	47/159	70/236	81/274				
70	43/169	62/244	69/272				
80	43/193	54/243	69/311				
90	39/197	54/289	69/350				
100	35/197	54/304	57/321				
120	35/236	46/311	57/385				
140	31/244	38/299	45/355				

Maximum Continuous Spliced Rail Length

Maximum Continuous Spliced Rail Length for SM Standard (ft.)/Maximum Reaction

	for SM Light (ft.)/Maximum Reaction Force (lbs) Attachment Spacing			
ΔT (°F)	24"	48"	72"	
40	51/115	70/157	81/182	
50	47/132	62/174	81/228	
60	43/145	54/182	69/233	
70	39/153	54/213	69/272	
80	35/157	46/207	57/257	
90	35/177	46/233	57/289	
100	31/174	46/259	57/321	
120	27/182	38/257	45/304	
140	27/213	38/299	45/355	

Flashloc Comp Mount

	Force (lbs)			
	Attachment Spacing			
ΔT (°F)	24"	48"	72"	
40	51/155	70/213	81/277	
50	47/179	62/236	69/262	
60	43/196	54/246	69/315	
70	39/208	54/288	57/304	
80	35/213	46/280	57/347	
90	35/240	46/333	57/390	
100	31/236	46/350	45/342	
120	27/246	38/347	45/411	
140	27/288	38/405	45/480	

	Maximum Continuous Spliced Rail Length for SM Light (ft.)/Maximum Reaction Force (lbs) Attachment Spacing			
ΔT (°F)	24"	48"	72"	
40	43/131	62/188	69/236	
50	39/148	54/205	69/262	
60	35/160	46/210	57/260	
70	31/165	46/245	57/304	
80	31/188	38/231	45/274	
90	27/185	38/260	45/308	
100	27/205	38/289	45/342	
120	23/210	30/274	33/301	
140	23/245	30/320	33/352	

NOTES:

The values displayed are the maximum allowed rail length, in feet, without a thermal break.

The installer is responsible for determining the maximum temperature difference (ΔT) used to establish the maximum rail length, without expansion joint, at the install location.

As spans increase, so does the maximum reaction force that the rail exerts on the L-foot. It is the responsibility of the installer to ensure that Maximum Reaction Force does not exceed the shear capacity of the roof connection.

ΔT refers to the maximum difference in the temperature of the rail between installation and the extreme high or low temperature. The Extreme Annual Design Conditions table at the following url can be used as a reference when determining ΔT.

http://ashrae-meteo.info/